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Canterbury City Council Head of Planning Military Road Canterbury CT1 1YW

Date:25 January 2021Your Ref:CA/20/01025Our Ref:SAH/2632/12224_Rev2CEmail:stephen@herringtonconsulting.co.uk

Discharge of Condition 3 for the proposed development at 53 Joy Lane, Whitstable, Kent, CT5 4DB (Unit C)

This letter has been prepared with reference to planning application CA/20/01025 and is aimed at discharging planning condition 3 (herein referred to as Condition 3) for the proposed development at the above address. Condition 3 relates to the safe management of both surface water runoff and foul drainage from the proposed development.

The combined proposal is for the erection of 3 new residential detached dwellings, on previously undeveloped land located on Joy Lane, Whitstable. This specific application is for the construction of Dwelling C.

The full details of the planning condition are quoted below:

Planning Condition 3

"...No development shall take place until details of the means of foul and surface water disposal, including a detailed sustainable surface water drainage scheme for the site, which is compliant with the Non-statutory Technical Standards for Sustainable Drainage (NTSS) and shall demonstrate the surface water runoff generated up to and including the 100yr critical storm (including allowance for climate change) will not exceed the runoff from the undeveloped site following the corresponding rainfall event, and so as not to increase the risk of flooding both on- or off-site, and including details for the long term maintenance of all surface water drainage infrastructure on site, and including the provision of measures to prevent the discharge of surface water onto the highway, have been submitted to and agreed in writing by the Local Planning Authority (LPA). The development shall be carried out in accordance with such details as are agreed and thereafter maintained..."

Herrington Consulting Limited

Canterbury Office Unit 6 & 7 Barham Business Park Elham Valley Road Barham Canterbury Kent CT4 6DQ

Tel 01227 833855

London Office Unit D Taper Building Weston Street London SE1 3QB

www.herringtonconsulting.co.uk

Co Reg No 5418977 VAT No 860 5179 20

Proposed Development

The proposed development is for the construction of 3 residential properties, an access road, and a parking area.

This report includes details of how Property C will be drained both in isolation and as part of the wider 3 unit scheme. This is to ensure that suitable provisions for surface water management are in place, in the event units A and B are not completed, or are completed at a later date, e.g., due to the phased nature of the development. Separate reports detailing the isolated drainage solution for properties A and B have also been produced and are to be submitted separately. Figure 1 below shows the proposed roof area for property C.

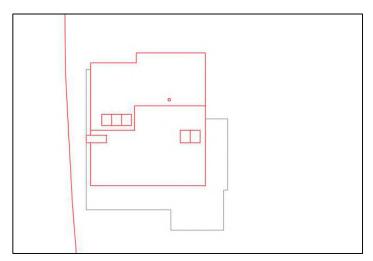


Figure 1 – Proposed plot C.

National Policy for SuDS

In accordance with the 2019 National Planning Policy Framework (NPPF), Sustainable Drainage Systems (SuDS) should be included within the proposed development scheme where it is practicable to do so. The proposed development must also maintain, or ideally reduce, the rate at which runoff is discharged offsite. This is to ensure that the offsite risk of surface water flooding is not increased by the development.

The proposed development will also need to comply with the Non-statutory Technical Standards for Sustainable Drainage Systems (NTSS) and as such, the NTSS has been referenced when devising the drainage system.

Lead Local Flood Authority (LLFA) Comments

Comments were provided by the LLFA on the 20th July 2020, and provide additional information on the level of detail required for Condition 3 to be discharged. This includes:

- Construction drawings or a tender document for the proposed drainage system, including details of the storage tank.
- Confirmation of existing capacity within the surface water sewer network for the area.
- Details of the maintenance strategy, including confirmation that the owners of the 3 properties will be tasked with the ongoing maintenance of the SuDS.

Climate Change

The NPPF (2019) and supporting Planning Practice Guidance Suite (2014) state that residential development should be considered for a minimum of 100 years. The Environment Agency (EA) provides guidance regarding the application of the climate change allowances relating to peak rainfall intensity and how they should be applied to the planning process. The recommended allowances for increases in peak rainfall intensity are applicable nationally and have therefore been considered. For this development, an increase of 40% has been applied to the peak rainfall to account for the impacts of climate change over the lifetime of the development.

Drainage Model and Calculations

A hydraulic model has been constructed for the proposed surface water drainage system using Causeway Flow + and hydrological data obtained from the Flood Estimation Handbook (FEH), via the Centre for Ecology and Hydrology online web portal.

The hydraulic model has been used to test the proposed drainage system for a series of rainfall events, with storm durations ranging from 15 minutes to 7 days, and return periods from 1:2 years, up to and including, the design rainfall event 1:100 years. A 40% increase in peak rainfall intensity has also been applied to the rainfall hyetographs to account for climate change.

Existing Drainage

The existing site has no known surface water drains. However, a survey carried out (by others) has confirmed a connection between the site and foul sewer within the adjacent road.

Asset location data has been obtained from the sewerage undertaker Southern Water (SW), which confirms the location of public sewerage infrastructure near to the site. Figure 2 below delineates the network of sewers for the area around Joy Lane.

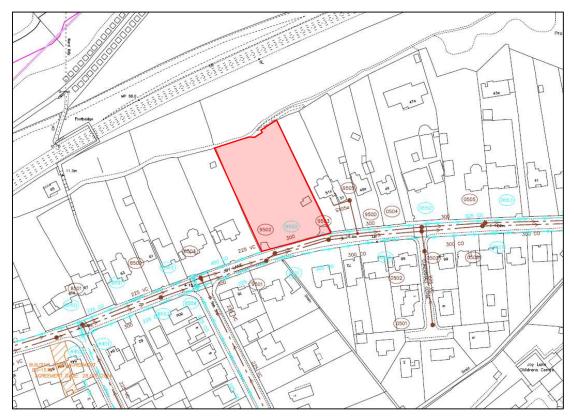


Figure 2 – Sewer mapping for the area around Joy Lane.

Greenfield runoff rates for the site have been calculated using the FEH Statistical Methodology, and are summarised in Table 1 below, along with calculations estimating the pre-development discharge rates based on the total area of existing hardstanding.

Return Period (years)	Greenfield Runoff Rate (I/s/ha)	Pre-development discharge rate based on 380 m ² of existing hardstanding (I/s)
1:2	2.3	7.2
1:10	4.2	14.1
1:30	6.2	18.7
1:100	8.2	24.0

Table 1 - Summary of greenfield and existing runoff rates for the site.

With the inclusion of additional impermeable areas onto the site, there will be an increase in the rate at which surface water runoff will be discharged from the site (pre-mitigation). In order to reduce this impact, SuDS will need to be incorporated into the development to ensure that the site complies with the NTSS and local planning policy.

Drainage Hierarchy and Opportunities for Managing Surface Water Runoff

The following opportunities for managing the surface water runoff discharged from the development site are listed in order of preference:

Infiltration – Infiltration testing has been undertaken by the applicant and the results confirm that ground conditions at the site are unsuitable for the use of infiltration SuDS. This option for draining the site has, therefore, been discounted.

Discharge to Watercourses – The nearest mapped watercourse is a small drain located across the public highway to the south of the site. In addition, this drain is located on land outside the applicant's control and does not appear to be connected to the other drainage features (e.g., surface water sewers) in this area. As a consequence, draining surface water runoff from the site into this drain is unlikely to be possible and this option for draining the site has therefore been discounted.

Discharge to Public Sewer System – There are several sewers within the road adjacent to the development site, which could facilitate a new surface water drainage connection to drain runoff from the development. On this basis, a connection to the public sewer system is likely to present the most viable solution for draining the development.

Measures to Prevent Discharge to the Highway

To prevent runoff from the site from draining to the highway, threshold drains will be incorporated into the drainage design for the access road into the development. These drainage channels will direct runoff into the SuDS for the site and will ensure that water does not leave the site during storms with return periods less than the design rainfall event. These drainage channels are shown on the detailed drainage drawing (Figure 2) below.

Drainage for Property C (In Isolation)

Assuming Property C is constructed in isolation from the 2 remaining units, the drainage system can still be constructed beneath the area that will eventually become the access road and parking for the dwellings. The drainage layout plan below shows how a large geo-cellular storage tank can be incorporated into the proposals to drain Property C and future proof the design for further development at a later date, so that units A and B can be constructed without the need for any upgrades to the capacity of the proposed storage tank.

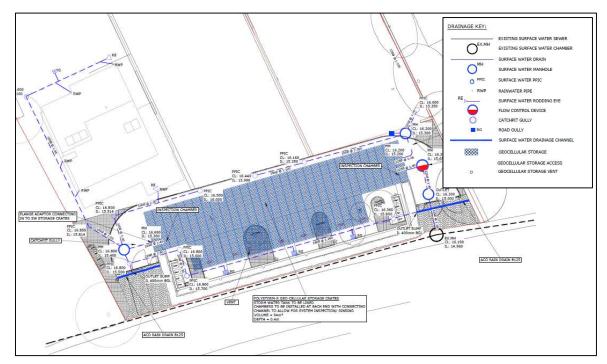


Figure 3 – Surface water drainage layout for Property C, Joy Lane, Whitstable.

Geo-Cellular Storage Tank – Runoff from Property C and the surrounding hardstanding and parking area will be drained to a storage tank located beneath the access drive and parking area. The design parameters for the geo-cellular storage tank are summarised in Table 2 below.

Parameter	Design (1:100yr+40%cc event)
Total impermeable area drainage to SuDS	1070 m ²
Urban creep allowance	10 %
Infiltration	Not permitted (high ground water and clay soils)
Porosity of storage tank	95 %
Dimensions of storage tank	~235m ² x 400mm (deep)
Required storage volume	~ 90 m³
Flow restriction device	Vortex flow control (2.0l/s)

Table 2 – Proposed drainage storage tank for a design of 1:100+ 40%cc.

Results from Hydraulic Model

The performance of the proposed drainage system has been tested by applying a series of rainfall events with varying return periods to a hydraulic model of the proposed drainage network. These calculations have been undertaken based on the combined 3 unit scheme, to ensure that on completion the storage

provided by the site will be sufficient. A range of storm durations have been applied to each of the return period scenarios to determine the peak runoff rates from the proposed development. The proposed drainage system has been modelled in Causeway Flow + V9.0, using the FEH2013 rainfall methodology.

If Property C is constructed prior to properties A and B, the total area draining to the storage system will be less than that used within the drainage model (discussed above). The consequence of this will be that the storage tank will have spare capacity during the design rainfall event and will therefore be less likely to surcharge. The results from this hydraulic model are summarised in Table 3 below.

Element	Surface water runoff calculations for a range of return period events for the pre- and post- developed scenarios						
	1:2yr	1:30yr	1:100yr				
Pre-development discharge	7.2 l/s	18.7 l/s	24.0 l/s				
Proposed discharge rate from storage tank, including 40% allowance for climate change	1.9 l/s	1.9 l/s	2.1 l/s				

Table 3 – Pre- and post- development surface water runoff calculations.

From Table 3 above and the model results appended, it is evident that with the inclusion of the proposed SuDS, there is potential to accommodate all of the surface water runoff from the site, up to and including the design rainfall event. This provides runoff characteristics which are closer to the greenfield runoff rates for the site and therefore, presents a betterment when compared to the existing situation. Consequently, it is considered that this will be acceptable to the LPA and LLFA.

Combined Site Drainage

A drainage layout plan for the 3 unit scheme has been produced (Figure 4 below), and shows how units A and B can be connected into the drainage network either as a single phase or in isolation.

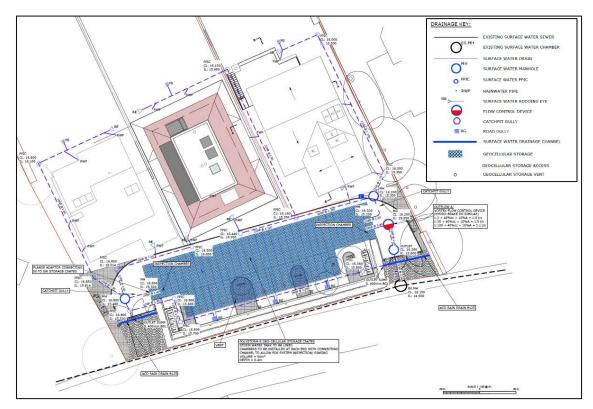


Figure 4 – Combined site drainage for the 3 unit scheme.

Existing Sewer Capacity

The sewerage undertaker has been contacted to determine the capacity of the existing sewerage infrastructure at the site, and to confirm whether the additional runoff from the proposed development can be accommodated within the existing surface water sewer network, without the need to upgrade the sewers in this area. The results of this capacity check have confirmed that there is currently adequate capacity for the proposed 2.11/s discharge, and a copy has been appended to this letter.

Design Exceedance

The proposed drainage system has been designed to accommodate surface water runoff generated under an extreme rainfall event, with a return period of 1 in 100 years, including a 40% increase in peak rainfall intensity (to account for the impacts of climate change). As such, this additional percentage increase complies with the EA's most contemporary guidance on climate change for the upper allowances.

Nonetheless, in the event of an exceedance scenario (i.e., an event which exceeds the design rainfall event), it is considered likely that water would back up within the drainage system and overflow to the rear of the properties, resulting in localised flooding within the gardens. Figure 5 below shows the proposed drainage system and likely pathways water will take as it flows across the site, in the event that the drainage system fails.

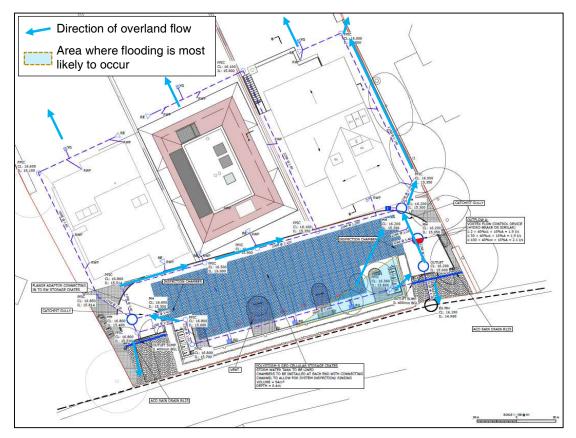


Figure 5 - Anticipated flow routes during an exceedance or blockage event.

In summary, with the inclusion of the SuDS discussed within this strategy, the proposed surface water drainage solution will not increase the risk of flooding at the site or within the surrounding area during an exceedance event and is therefore considered appropriate.

Maintenance and Management

A maintenance and management plan for the drainage system and SuDS has been prepared, and a copy is appended to this document.

It is envisaged that each of the property owners / occupants will be tasked with the ongoing maintenance of the drainage system. As a result, for Property C in isolation, maintenance for the entire drainage system would be tasked to the occupants / property owner. As additional units are constructed, agreements would need to be put in place to ensure responsibility for maintaining the SuDS is spread across all of the land owners / occupiers. As a result, drains lying within private land ownership will remain the responsibility of the individual property owner, with the communal elements of the drainage system being maintained as part of an agreement between all 3 property owners.

Management of Foul Water

In general, there are two methods for draining effluent from proposed developments. The preferred solution is a connection to the public sewer network, which is controlled by the sewerage undertaker. Nonetheless, if there are no sewers located near to the development site or if there are particular reasons why a connection to the public sewer system would not be possible, e.g., topography, cost, environmental concerns etc., then the use of package treatment systems or cesspits will be permitted.

In this case, the nearest public sewers to the site are located beneath the adjacent road (Joy Lane). The SW sewer mapping shows that there are two foul sewers located beneath this road and evidence from onsite investigations, undertaken by others, has confirmed that an existing foul drainage connection from the site to one of these sewers is present. A connection to the existing foul sewer system will therefore be the most viable solution for draining foul wastewater from the proposed development.

The peak rate at which foul wastewater is discharged from property C is 0.05l/s. Given the relatively low flow rate, it is considered unlikely that the additional foul wastewater discharged from the property will have a significant impact on the sewer system, or increase the risk of sewer flooding in this area.

A pre-development enquiry has been undertaken with SW to confirm the capacity of the existing foul sewer network at the site and ensure that it is suitable for up to 3 additional units, with a combined flow rate of ~0.14l/s. The results of this enquiry confirm that there is sufficient capacity within the existing network to accommodate wastewater from the 3 new dwellings. Consequently, capacity for Property C will be available irrespective of whether it is constructed in isolation or as part of the wider 3 unit development.

<u>Summary</u>

The opportunities for draining surface water runoff and foul wastewater from the proposed development of both Plot C and the 3 unit scheme at Joy Lane, Whitstable have been assessed, with the aim of discharging Condition 3.

The analysis has shown that discharging surface water runoff into the existing public sewer system will present the most viable solution for draining the site. A large geo-cellular storage tank has been incorporated into the drainage system for the development, in order to provide storage for stormwater. This tank has been designed to manage runoff from the 3 unit scheme but is still appropriate for use in managing runoff from the single dwelling.

The results of the hydraulic drainage model for the proposed drainage system confirm that the proposed SuDS have sufficient capacity to store runoff from the entire design rainfall event, with a return period of 1:100 years, including a 40% increase in peak rainfall intensity to account for climate change. The peak discharge rate under this scenario is limited to a rate of 2.11/s. As a consequence, the proposals meet the requirements of both the NTSS and the NPPF.

Construction drawings for the proposed drainage system have been prepared, alongside an indicative drawing showing plot C and the storage tank in isolation. A copy of these drawings is appended to this report.

Maintenance and management schedules for the proposed SuDS are included within a maintenance plan that has been prepared for the development, a copy of which is appended to this document.

The opportunities for disposing foul wastewater from the site have also been considered, and calculations have been undertaken to estimate the increase in foul wastewater discharged offsite. The appraisal demonstrates that the most viable solution is to connect into the existing foul sewer network located in Joy Lane.

Confirmation of the foul and surface water sewer networks capacity has been obtained from the sewerage undertaker and following the discharge of Condition 3, approval for any new sewer connection(s) will need to be obtained from the sewerage undertaker.

The information contained within this document provides details to demonstrate how surface water runoff and foul effluent will be managed on site, and addresses the comments raised by the LLFA. I trust that this information will be sufficient to enable Condition 3 to be discharged in full.

Yours faithfully,

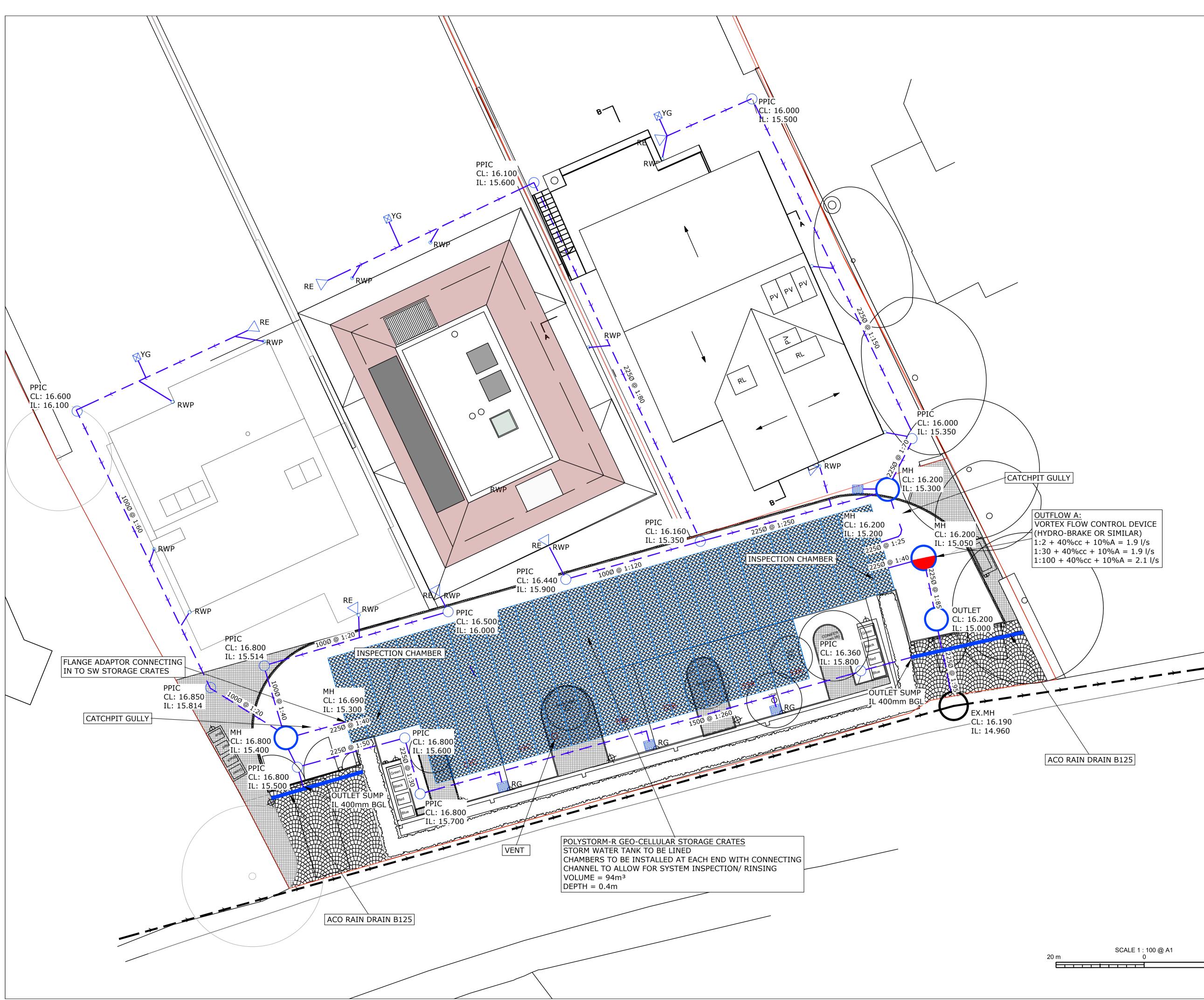
Stephen Hayward BSc (Hons) ARSM MCIWEM Senior Drainage Analyst

Enclosed documents:

- Drainage Details
- Causeway Flow+ Calculations
- SuDS Maintenance Plan
- Southern Water Correspondence



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GENERAL NOTES

1. THIS DRAWING IS TO BE READ IN CONJUNCTION WITH ALL RELEVANT ENGINEERS, ARCHITECTS AND SPECIALISTS DRAWINGS AND THE SPECIFICATION.

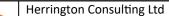
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- 2. ALL WORK IS TO BE CARRIED OUT IN ACCORDANCE WITH THE RELEVANT BRITISH STANDARDS, EUROPEAN NORMS, CODES OF PRACTICE AND BUILDING PRACTICE.
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- INFILTRATION TESTING AND TRIAL HOLES. 5. ALL DRAINAGE SYSTEMS WILL NEED TO BE INSTALLED AND DESIGNED FOR
- SUITABLE LOADING REQUIREMENTS. 6. THE CONTRACTOR SHALL OBTAIN PRIOR APPROVAL AND ALL NECESSARY
- LICENCES FROM THE THE HIGHWAY AUTHORITY AND/OR SEWERAGE UNDERTAKER BEFORE CARRYING OUT ANY WORKS.

DRAINAGE KEY:



20 m





Page 1

Design Settings

Rainfall Methodology	FEH-13	Maximum Time of Concentration (mins)	30.00	Preferred Cover Depth (m)	1.200
Return Period (years)	100	Maximum Rainfall (mm/hr)	200.0	Include Intermediate Ground	\checkmark
Additional Flow (%)	10	Minimum Velocity (m/s)	1.00	Enforce best practice design rules	х
CV	1.000	Connection Type	Level Soffits		
Time of Entry (mins)	4.00	Minimum Backdrop Height (m)	0.200		

<u>Nodes</u>

Name	Area (ha)	T of E (mins)	Cover Level (m)	Diameter (mm)	Width (mm)	Easting (m)	Northing (m)	Depth (m)
8	0.004	4.00	16.800	650		1093.000	16.000	1.286
9	0.003	4.00	16.500	650		1103.000	19.000	0.500
10	0.004	4.00	16.850	650		1090.000	16.000	1.036
Storage Tank	0.000	4.00	16.400	1500		1111.182	18.220	1.300
Flow Control Device	0.000	4.00	16.200	1350		1130.000	23.000	1.150
Outlet	0.000	4.00	16.200	1200		1131.000	19.000	1.200
1	0.003	4.00	16.300	650	400	1130.000	17.000	0.450
2			16.360	650		1127.000	16.000	0.560
3	0.033	4.00	16.800	650		1102.000	9.000	1.100
4			16.800	650		1101.000	12.000	1.200
5			16.800	650		1096.000	11.000	1.300
6	0.009	4.00	16.900	200	400	1095.989	9.796	0.500
7			16.800	1200		1095.963	12.252	1.400
11	0.005	4.00	16.100	650		1107.000	41.000	0.500
12	0.012	4.00	16.160	650		1116.000	23.000	0.810
13	0.013	4.00	16.200	1200		1128.103	26.084	0.900
14	0.009	4.00	16.000	650		1130.000	29.000	0.650
15	0.005	4.00	16.000	650		1120.128	49.000	0.500
16			16.690	800		1097.846	12.736	1.390
17			16.160	1200		1128.593	24.782	0.960
18	0.006	4.00	16.600	650		1082.386	31.211	0.500
19	0.005	4.00	16.440	650		1110.000	22.000	0.540
Existing Surface Water Sewer			16.190	1200		1132.214	15.396	1.210



<u>Links</u>

Name	US Node	DS Node	Length (m)	ks (mm) / n	US IL (m)	DS IL (m)	Fall (m)	Slope (1:X)	Dia (mm)	T of C (mins)	Rain (mm/hr)
1.000	1	2	3.162	0.060	15.850	15.800	0.050	63.2	150	4.03	165.0
1.001	2	3	25.962	0.060	15.800	15.700	0.100	259.6	150	4.60	165.0
1.002	3	4	3.162	0.060	15.700	15.600	0.100	31.6	225	4.62	165.0
1.007	Storage Tank	Flow Control Device	19.416	0.060	15.100	15.050	0.050	388.3	375	5.14	163.5
1.008	Flow Control Device	Outlet	4.123	0.600	15.050	15.030	0.020	206.2	150	5.24	162.4
1.003	4	5	5.099	0.060	15.600	15.500	0.100	51.0	225	4.66	165.0
2.000	6	5	1.204	0.060	16.400	16.300	0.100	12.0	100	4.01	165.0
1.004	5	7	1.253	0.060	15.500	15.400	0.100	12.5	225	4.66	165.0
4.001	8	7	4.778	0.060	15.514	15.400	0.114	41.9	100	4.13	165.0
1.005	7	16	1.944	0.060	15.400	15.300	0.100	19.4	225	4.67	165.0
1.006	16	Storage Tank	14.420	0.060	15.300	15.200	0.100	144.2	225	4.85	165.0
4.000	9	8	10.440	0.060	16.000	15.514	0.486	21.5	100	4.08	165.0
3.001	10	7	7.043	0.060	15.814	15.450	0.364	19.3	100	4.27	165.0
7.001	14	13	3.479	0.060	15.350	15.300	0.050	69.6	225	4.31	165.0

Name	Vel (m/s)	Cap (I/s)	Flow (l/s)	US Depth (m)	DS Depth (m)	Σ Area (ha)	Σ Add Inflow (I/s)	Pro Depth (mm)	Pro Velocity (m/s)
1.000	1.609	28.4	2.0	0.300	0.410	0.003	0.0	27	0.933
1.001	0.761	13.5	2.0	0.410	0.950	0.003	0.0	39	0.545
1.002	2.982	118.6	23.6	0.875	0.975	0.036	0.0	67	2.343
1.007	1.111	122.7	72.1	0.925	0.775	0.111	0.0	207	1.154
1.008	0.696	12.3	71.7	1.000	1.020	0.111	0.0	150	0.709
1.003	2.329	92.6	23.6	0.975	1.075	0.036	0.0	77	1.957
2.000	2.945	23.1	5.9	0.400	0.400	0.009	0.0	34	2.464
1.004	4.797	190.8	29.5	1.075	1.175	0.045	0.0	59	3.539
4.001	1.538	12.1	4.6	1.186	1.300	0.007	0.0	43	1.433
1.005	3.830	152.3	40.7	1.175	1.165	0.062	0.0	79	3.262
1.006	1.353	53.8	40.7	1.165	0.975	0.062	0.0	146	1.481
4.000	2.181	17.1	2.0	0.400	1.186	0.003	0.0	23	1.474
3.001	2.303	18.1	6.6	0.936	1.250	0.010	0.0	42	2.130
7.001	1.981	78.8	9.2	0.425	0.675	0.014	0.0	51	1.340

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<u>Links</u>

Name	US Node	DS Node	Length (m)	ks (mm) / n	US IL (m)	DS IL (m)	Fall (m)	Slope (1:X)	Dia (mm)	T of C (mins)	Rain (mm/hr)
5.001	12	13	12.490	0.060	15.350	15.300	0.050	249.8	225	4.39	165.0
5.002	13	17	1.391	0.060	15.300	15.200	0.100	13.9	225	4.39	165.0
5.003	17	Storage Tank	18.607	0.060	15.200	15.100	0.100	186.1	225	4.66	165.0
5.000	11	12	20.125	0.060	15.600	15.350	0.250	80.5	225	4.18	165.0
7.000	15	14	22.304	0.060	15.500	15.350	0.150	148.7	225	4.28	165.0
3.000	18	10	17.010	0.060	16.100	15.814	0.286	59.5	100	4.22	165.0
6.000	19	12	6.083	0.060	15.900	15.850	0.050	121.7	100	4.12	165.0
1.009	Outlet	Existing Surface Water Sewer	3.803	0.600	15.000	14.980	0.020	190.2	225	5.42	50.0

Name	Vel	Сар	Flow	US	DS	Σ Area	Σ Add	Pro	Pro
	(m/s)	(I/s)	(I/s)	Depth	Depth	(ha)	Inflow	Depth	Velocity
				(m)	(m)		(I/s)	(mm)	(m/s)
5.001	1.012	40.2	14.4	0.585	0.675	0.022	0.0	93	0.929
5.002	4.547	180.8	32.1	0.675	0.735	0.049	0.0	64	3.482
5.003	1.183	47.0	32.1	0.735	1.075	0.049	0.0	137	1.270
5.000	1.836	73.0	3.3	0.275	0.585	0.005	0.0	32	0.939
7.000	1.331	52.9	3.3	0.275	0.425	0.005	0.0	37	0.741
3.000	1.279	10.0	3.9	0.400	0.936	0.006	0.0	43	1.201
6.000	0.874	6.9	3.3	0.440	0.210	0.005	0.0	49	0.866
1.009	0.945	37.6	22.1	0.975	0.985	0.111	0.0	124	0.982

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Pipeline Schedule

Link	Length (m)	Slope (1:X)	Dia (mm)	Link Type	US CL (m)	US IL (m)	US Depth (m)	DS CL (m)	DS IL (m)	DS Depth (m)
1.000	3.162	63.2	150	Circular	16.300	15.850	0.300	16.360	15.800	0.410
1.001	25.962	259.6	150	Circular	16.360	15.800	0.410	16.800	15.700	0.950
1.002	3.162	31.6	225	Circular	16.800	15.700	0.875	16.800	15.600	0.975
1.007	19.416	388.3	375	Circular	16.400	15.100	0.925	16.200	15.050	0.775
1.008	4.123	206.2	150	Circular	16.200	15.050	1.000	16.200	15.030	1.020
1.003	5.099	51.0	225	Circular	16.800	15.600	0.975	16.800	15.500	1.075
2.000	1.204	12.0	100	Circular	16.900	16.400	0.400	16.800	16.300	0.400
1.004	1.253	12.5	225	Circular	16.800	15.500	1.075	16.800	15.400	1.175
4.001	4.778	41.9	100	Circular	16.800	15.514	1.186	16.800	15.400	1.300
1.005	1.944	19.4	225	Circular	16.800	15.400	1.175	16.690	15.300	1.165
1.006	14.420	144.2	225	Circular	16.690	15.300	1.165	16.400	15.200	0.975
4.000	10.440	21.5	100	Circular	16.500	16.000	0.400	16.800	15.514	1.186
3.001	7.043	19.3	100	Circular	16.850	15.814	0.936	16.800	15.450	1.250
7.001	3.479	69.6	225	Circular	16.000	15.350	0.425	16.200	15.300	0.675
5.001	12.490	249.8	225	Circular	16.160	15.350	0.585	16.200	15.300	0.675

Link	US	Dia	Width	Node	MH	DS	Dia	Node	MH
	Node	(mm)	(mm)	Туре	Туре	Node	(mm)	Туре	Туре
1.000	1	650	400	Manhole	Adoptable	2	650	Manhole	Adoptable
1.001	2	650		Manhole	Adoptable	3	650	Manhole	Adoptable
1.002	3	650		Manhole	Adoptable	4	650	Manhole	Adoptable
1.007	Storage Tank	1500		Manhole	Adoptable	Flow Control Device	1350	Manhole	Adoptable
1.008	Flow Control Device	1350		Manhole	Adoptable	Outlet	1200	Manhole	Adoptable
1.003	4	650		Manhole	Adoptable	5	650	Manhole	Adoptable
2.000	6	200	400	Manhole	Adoptable	5	650	Manhole	Adoptable
1.004	5	650		Manhole	Adoptable	7	1200	Manhole	Adoptable
4.001	8	650		Manhole	Adoptable	7	1200	Manhole	Adoptable
1.005	7	1200		Manhole	Adoptable	16	800	Manhole	Adoptable
1.006	16	800		Manhole	Adoptable	Storage Tank	1500	Manhole	Adoptable
4.000	9	650		Manhole	Adoptable	8	650	Manhole	Adoptable
3.001	10	650		Manhole	Adoptable	7	1200	Manhole	Adoptable
7.001	14	650		Manhole	Adoptable	13	1200	Manhole	Adoptable
5.001	12	650		Manhole	Adoptable	13	1200	Manhole	Adoptable

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Pipeline Schedule

Link	Length (m)	Slope (1:X)	Dia (mm)	Link Type	US CL (m)	US IL (m)	US Depth (m)	DS CL (m)	DS IL (m)	DS Depth (m)
5.002	1.391	13.9	225	Circular	16.200	15.300	0.675	16.160	15.200	0.735
5.003	18.607	186.1	225	Circular	16.160	15.200	0.735	16.400	15.100	1.075
5.000	20.125	80.5	225	Circular	16.100	15.600	0.275	16.160	15.350	0.585
7.000	22.304	148.7	225	Circular	16.000	15.500	0.275	16.000	15.350	0.425
3.000	17.010	59.5	100	Circular	16.600	16.100	0.400	16.850	15.814	0.936
6.000	6.083	121.7	100	Circular	16.440	15.900	0.440	16.160	15.850	0.210
1.009	3.803	190.2	225	Circular	16.200	15.000	0.975	16.190	14.980	0.985

Link	US	Dia	Width	Node	МН	DS	Dia	Node	МН
	Node	(mm)	(mm)	Туре	Туре	Node	(mm)	Туре	Туре
5.002	13	1200		Manhole	Adoptable	17	1200	Manhole	Adoptable
5.003	17	1200		Manhole	Adoptable	Storage Tank	1500	Manhole	Adoptable
5.000	11	650		Manhole	Adoptable	12	650	Manhole	Adoptable
7.000	15	650		Manhole	Adoptable	14	650	Manhole	Adoptable
3.000	18	650		Manhole	Adoptable	10	650	Manhole	Adoptable
6.000	19	650		Manhole	Adoptable	12	650	Manhole	Adoptable
1.009	Outlet	1200		Manhole	Adoptable	Existing Surface Water Sewer	1200	Manhole	Adoptable

Manhole Schedule

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Width (mm)	Connectior	ıs	Link	IL (m)	Dia (mm)
8	1093.000	16.000	16.800	1.286	650			1	4.000	15.514	100
							\mathbb{Q}^{1}				
							0	0	4.001	15.514	100
9	1103.000	19.000	16.500	0.500	650						
							0				
								0	4.000	16.000	100

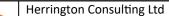
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Manhole Schedule

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Width (mm)	Connections	Link	IL (m)	Dia (mm)
10	1090.000	16.000	16.850	1.036	650			3.000	15.814	100
							0	3.001	15.814	100
Storage Tank	1111.182	18.220	16.400	1.300	1500		1	5.003	15.100	225
							2 50 2	1.006	15.200	225
							0		15.100	375
Flow Control Device	1130.000	23.000	16.200	1.150	1350		1	1.007	15.050	375
							0 V	1.008	15.050	150
Outlet	1131.000	19.000	16.200	1.200	1200			1.008	15.030	150
							0	1.009	15.000	225
1	1130.000	17.000	16.300	0.450	650	400				
							oct			
							0		15.850	150
2	1127.000	16.000	16.360	0.560	650		1	1.000	15.800	150
							0	1.001	15.800	150
3	1102.000	9.000	16.800	1.100	650			-	15.700	150
							0	1.002	15.700	225
4	1101.000	12.000	16.800	1.200	650		1	_	15.600	225
								1.003	15.600	225





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Manhole Schedule

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Width (mm)	Connection	IS	Link	IL (m)	Dia (mm)
5	1096.000	11.000	16.800	1.300	650		0	1	2.000	16.300	100
							— 2	2	1.003	15.500	225
							1	0	1.004	15.500	225
6	1095.989	9.796	16.900	0.500	200	400					
								0	2.000	16.400	100
7	1095.963	12.252	16.800	1.400	1200		1	1	4.001	15.400	100
							2 >0	2	3.001	15.450	100
							Ψ	3	1.004	15.400	225
							3	0	1.005	15.400	225
11	1107.000	41.000	16.100	0.500	650						
							\bigcirc				
							ž	0	5.000	15.600	225
12	1116.000	23.000	16.160	0.810	650		2	1	6.000	15.850	100
							1	2	5.000	15.350	225
								0	5.001	15.350	225
13	1128.103	26.084	16.200	0.900	1200		1	1	7.001	15.300	225
							2-0	2	5.001	15.300	225
							No.	0	5.002	15.300	225
14	1130.000	29.000	16.000	0.650	650		1	1	7.000	15.350	225
							\bigcirc				
							oK	0	7.001	15.350	225
15	1120.128	49.000	16.000	0.500	650		\bigcirc				
							, S	0	7.000	15.500	225

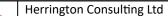
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Manhole Schedule

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Width (mm)	Connections	Link	IL (m)	Dia (mm)	
16	1097.846	12.736	16.690	1.390	800	<u> </u>	1	1.005	15.300	225	
								1.006	15.300	225	
17	1128.593	24.782	16.160	0.960	1200			5.002	15.200	225	
							C	5.003	15.200	225	
18	1082.386	31.211	16.600	0.500	650						
19	1110.000	22.000	16.440	0.540	650		<u>°</u> C	3.000	16.100	100	
19	1110.000	22.000	10.440	0.540	050		⊖→0				
							C	6.000	15.900	100	
Existing Surface Water Sewer	1132.214	15.396	16.190	1.210	1200			1.009	14.980	225	
			<u>Simula</u>	ation Sett	<u>ings</u>		1	I			
Rainfall Methodol Summer	CV 1.000		Skip Stea	sis Speed ady State	Detail x	ed A	Additional Storage Check Discharge	Rate(s)	20.0 x		
Winter	CV 1.000	Drain	Down Tin	ne (mins)	240		Check Discharge	Volume	х		
15 30	Storm Durations 15 30 60 120 180 240 360 480 600 720 960 1440										

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	Herrington Consulting Ltd	Netwo	alcs A Rev 2.pfd ork: Storm Networ en Hayward /2020	k	Page 9
	Return Period Clin (years) 100	-		onal Flow Q %) O	
	Node Flow Co	ontrol Device Online H	lydro-Brake [®] Cont	<u>rol</u>	
Re	Flap Valve x places Downstream Link √ Invert Level (m) 15.050 Design Depth (m) 0.800 Design Flow (I/s) 2.0	Sump	Available x : Number CTL-CH neter (m) 0.100	linimise upstream stora IE-0068-2000-0800-200	
	Node Stor	age Tank Depth/Area	Storage Structure		
	e Inf Coefficient (m/hr) 0.00000 e Inf Coefficient (m/hr) 0.00000		2.0 0.96 Time to h	Invert Level (m) 15.2 alf empty (mins)	.00
	Depth Area Inf Area (m) (m ²) (m ²) 0.000 235.0 0.0	-	f Area Depth (m ²) (m) 0.0 0.401	Area Inf Area (m ²) (m ²) 0.0 0.0	
	Flow+ v10 1 Conv	right © 1988-2020 Ca	useway Technolog	ies Itd	

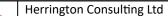




Results for 100 year +40% CC +10% A Critical Storm Duration. Lowest mass balance: 99.87%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
600 minute winter	8	555	15.943	0.429	0.7	0.1715	0.0000	SURCHARGED
15 minute summer	9	10	16.026	0.026	2.9	0.0122	0.0000	ОК
600 minute winter	10	555	15.943	0.129	1.0	0.0537	0.0000	SURCHARGED
600 minute winter	Storage Tank	555	15.943	0.843	16.2	91.8415	0.0000	SURCHARGED
600 minute winter	Flow Control Device	555	15.942	0.892	6.8	1.2772	0.0000	FLOOD RISK
600 minute winter	Outlet	555	15.038	0.038	2.1	0.0433	0.0000	ОК
600 minute winter	1	555	15.943	0.093	0.3	0.0377	0.0000	ОК
600 minute winter	2	555	15.943	0.143	0.3	0.0474	0.0000	ОК
600 minute winter	3	555	15.943	0.243	3.5	0.2407	0.0000	SURCHARGED
600 minute winter	4	555	15.943	0.343	6.6	0.1138	0.0000	SURCHARGED
600 minute winter	5	555	15.943	0.443	4.4	0.1470	0.0000	SURCHARGED
15 minute summer	6	10	16.465	0.065	8.8	0.0307	0.0000	ОК
600 minute winter	7	555	15.943	0.543	6.1	0.6137	0.0000	SURCHARGED
600 minute winter	11	555	15.943	0.343	0.5	0.1891	0.0000	FLOOD RISK
600 minute winter	12	555	15.943	0.593	2.2	0.3900	0.0000	FLOOD RISK

Link Event	US	Link	DS	Outflow	Velocity	Flow/Cap	Link	Discharge
(Upstream Depth)	Node		Node	(I/s)	(m/s)		Vol (m³)	Vol (m³)
600 minute winter	8	4.001	7	0.7	0.517	0.058	0.0374	
15 minute summer	9	4.000	8	2.9	0.923	0.169	0.0494	
600 minute winter	10	3.001	7	1.0	1.308	0.055	0.0551	
600 minute winter	Storage Tank	1.007	Flow Control Device	-6.9	0.173	-0.056	2.1415	
600 minute winter	Flow Control Device	Hydro-Brake [®]	Outlet	2.1				
600 minute winter	Outlet	1.009	Existing Surface Water Sewer	2.1	0.494	0.056	0.0163	74.8
600 minute winter	1	1.000	2	0.3	0.447	0.011	0.0454	
600 minute winter	2	1.001	3	0.3	0.215	0.023	0.4530	
600 minute winter	3	1.002	4	3.5	1.163	0.030	0.1258	
600 minute winter	4	1.003	5	-4.1	1.175	-0.044	0.2028	
600 minute winter	5	1.004	7	4.4	1.499	0.023	0.0498	
15 minute summer	6	2.000	5	8.8	2.117	0.380	0.0050	
600 minute winter	7	1.005	16	12.4	1.246	0.081	0.0773	
600 minute winter	11	5.000	12	0.5	0.240	0.007	0.8004	
600 minute winter	12	5.001	13	2.2	0.727	0.055	0.4967	





Results for 100 year +40% CC +10% A Critical Storm Duration. Lowest mass balance: 99.87%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
600 minute winter	13	555	15.943	0.643	4.9	0.9311	0.0000	FLOOD RISK
600 minute winter	14	555	15.943	0.593	2.5	0.3769	0.0000	FLOOD RISK
600 minute winter	15	555	15.943	0.443	0.6	0.2443	0.0000	FLOOD RISK
600 minute winter	16	555	15.943	0.643	12.4	0.3232	0.0000	SURCHARGED
600 minute winter	17	555	15.943	0.743	18.8	0.8398	0.0000	FLOOD RISK
15 minute summer	18	10	16.153	0.053	5.8	0.0316	0.0000	ОК
15 minute summer	19	10	15.965	0.065	4.9	0.0347	0.0000	ОК
600 minute winter	Existing Surface Water Sewer	555	15.016	0.036	2.1	0.0000	0.0000	ОК

Link Event	US	Link	DS	Outflow	Velocity	Flow/Cap	Link	Discharge
(Upstream Depth)	Node		Node	(I/s)	(m/s)		Vol (m³)	Vol (m³)
600 minute winter	13	5.002	17	18.8	1.093	0.104	0.0553	
600 minute winter	14	7.001	13	1.7	0.686	0.022	0.1384	
600 minute winter	15	7.000	14	0.5	0.370	0.009	0.8871	
600 minute winter	16	1.006	Storage Tank	6.3	0.905	0.117	0.5735	
600 minute winter	17	5.003	Storage Tank	5.1	0.754	0.108	0.7400	
15 minute summer	18	3.000	10	5.8	1.393	0.578	0.0715	
15 minute summer	19	6.000	12	4.9	0.989	0.714	0.0301	

herrington CONSULTING

Maintenance and Management Plan for the Drainage at Joy Lane, Whitstable.

Date:18 September 2020Your Ref:CA/19/00456Our Ref:SAH/2632/10909_MEmail:stephen@herringtonconsulting.co.uk

Maintenance Plan for the Sustainable Drainage System at Joy Lane, Whitstable.

Introduction

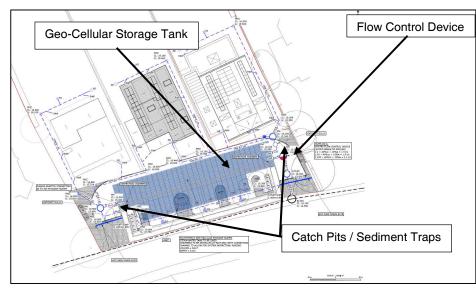
The proposed drainage network at Joy Lane, Whitstable, comprises a Sustainable Drainage System (SuDS), in addition to the more traditional piped drainage system. The maintenance requirements may therefore differ from a site which is solely drained using a traditional piped drainage system.

What are SuDS?

SuDS are drainage features designed to replicate natural processes of runoff and reduce the risk of flooding, as well as provide benefits to biodiversity and ecology. Integrating water into developments using SuDS can also provide benefits to the amenity of a site, creating nicer places for people to live.

Details of the proposed Drainage System

The drainage layout plan showing the location of the proposed SuDS is appended to this document, and the key drainage features are labelled on Figure 1 (below).



Herrington Consulting Limited

Canterbury Office

Unit 6 & 7 Barham Business Park Elham Valley Road Barham Canterbury Kent CT4 6DQ

Tel 01227 833855

London Office Unit D Taper Building Weston Street London SE1 3QB

www.herringtonconsulting.co.uk

Figure 1 – Plan showing the proposed SuDS that will need to be maintained.

The drainage system at Joy Lane consists of a piped drainage network, geocellular storage tank, flow control device, sediment traps, gullies, and linear drainage channels. Each of these elements of the drainage system will require different maintenance.

Maintenance Responsibilities

For any private drainage within the curtilage of each property the responsibility for the continued maintenance will belong solely to the owner of the property.

For the communal elements of the drainage system, including any lateral drains, the responsibility for maintenance will be tasked to all three property owners. This includes the inspection and maintenance of the geo-cellular storage tank. An agreement will need to be drawn up between the property owners to ensure continued maintenance is carried out. The final copy of this maintenance plan should be provided to each of the owners / occupants of the properties to ensure they are aware of their responsibilities with regard to the maintenance of any SuDS.

Maintenance and Management Requirements

Regular maintenance for the drainage system must be carried out to ensure continued performance of the drainage system: Maintenance schedules for the SuDS and drainage components are appended to this document. These schedules include typical inspection frequencies which should be adjusted after the first few years following installation, to account for more or less frequent maintenance and inspection depending on how the drainage system performs after this bedding in period.

List of maintenance schedules included:

- Geo-Cellular Storage
- Flow Control Device
- Pipework
- Sediment Traps / Catchpits
- Road Gullies
- Linear Drainage Channels
- Manholes
- PPIC's

Following construction, manufacturer-specific maintenance requirements must also be appended to this document.

Contact Details

Contact details for all manufactures should be included within the final maintenance and management plan for the site, which will need to be provided to the site occupants. At present, the following contact information is known:

Designers: Herrington Consulting Limited

- Email: enquiries@herringtonconsulting.co.uk
- Telephone: 01227 833855
- Website: <u>www.herringtonconsulting.co.uk</u>

Lead Local Flood Authority: Kent County Council

Email: <u>SuDS@kent.gov.uk</u>

To be contacted if changes to the drainage system are proposed following construction.

Sewerage undertaker: Southern Water

Website Advice: www.southernwater.co.uk/help-advice/what-to-do-in-an-emergency

To be contacted if flooding from the sewer network offsite occurs, or if changes to the drainage system are to be made.

Flow Control Device: Manufacturer TBC

Geo-Cellular Storage Crates: Manufacturer TBC

Emergency Action

-

<u>Spillages:</u> The outfall from the drainage system discharges into a Southern Water public sewer. Any accidental spillage of pollutants, such as; oils, spirits, etc. could result in contamination reaching the sewer network. If a spillage or accident occurs it is recommended that the outlets from the site are closed as soon as possible to reduce the potential for contamination to be discharged offsite. The Environment Agency should be informed of the spillage as soon as possible via their incident reporting service and should be contacted during the clean-up and remediation operations. Further advice can be obtained from https://www.gov.uk/report-an-environmental-incident

<u>Flooding</u>: If residents or maintenance personnel notice evidence of the drainage system failing e.g. from visible flooding or deformation of the land surface around pipes, manholes, or geo-cellular storage crates, the contractor responsible for installing the drainage system should be contacted as soon as possible to provide advice. It may also be necessary to contact the manufacturer of the geo-cellular storage tank and flow control device, and the designers of the drainage system. Inspections should also be carried out to determine the source of the failure.

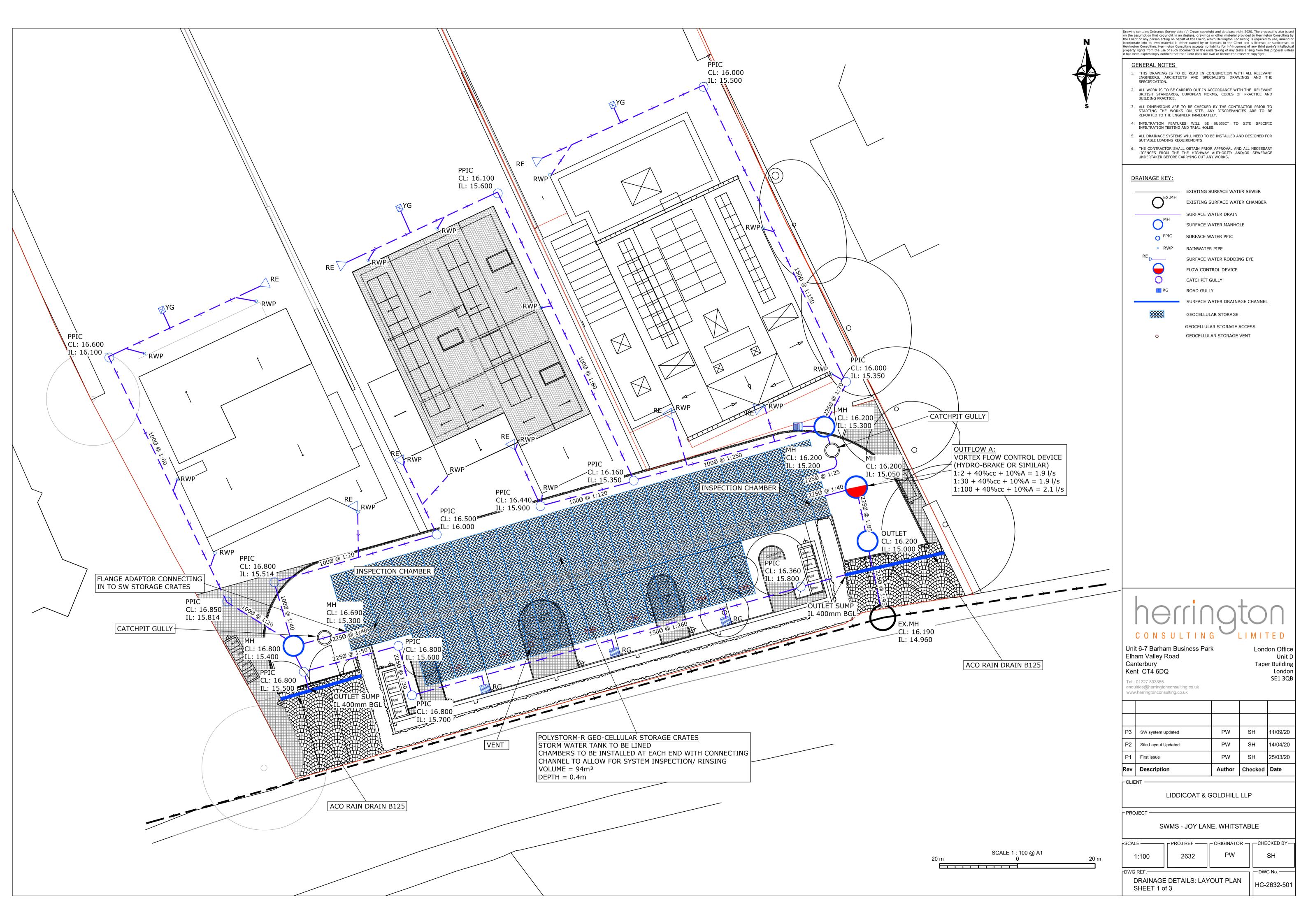
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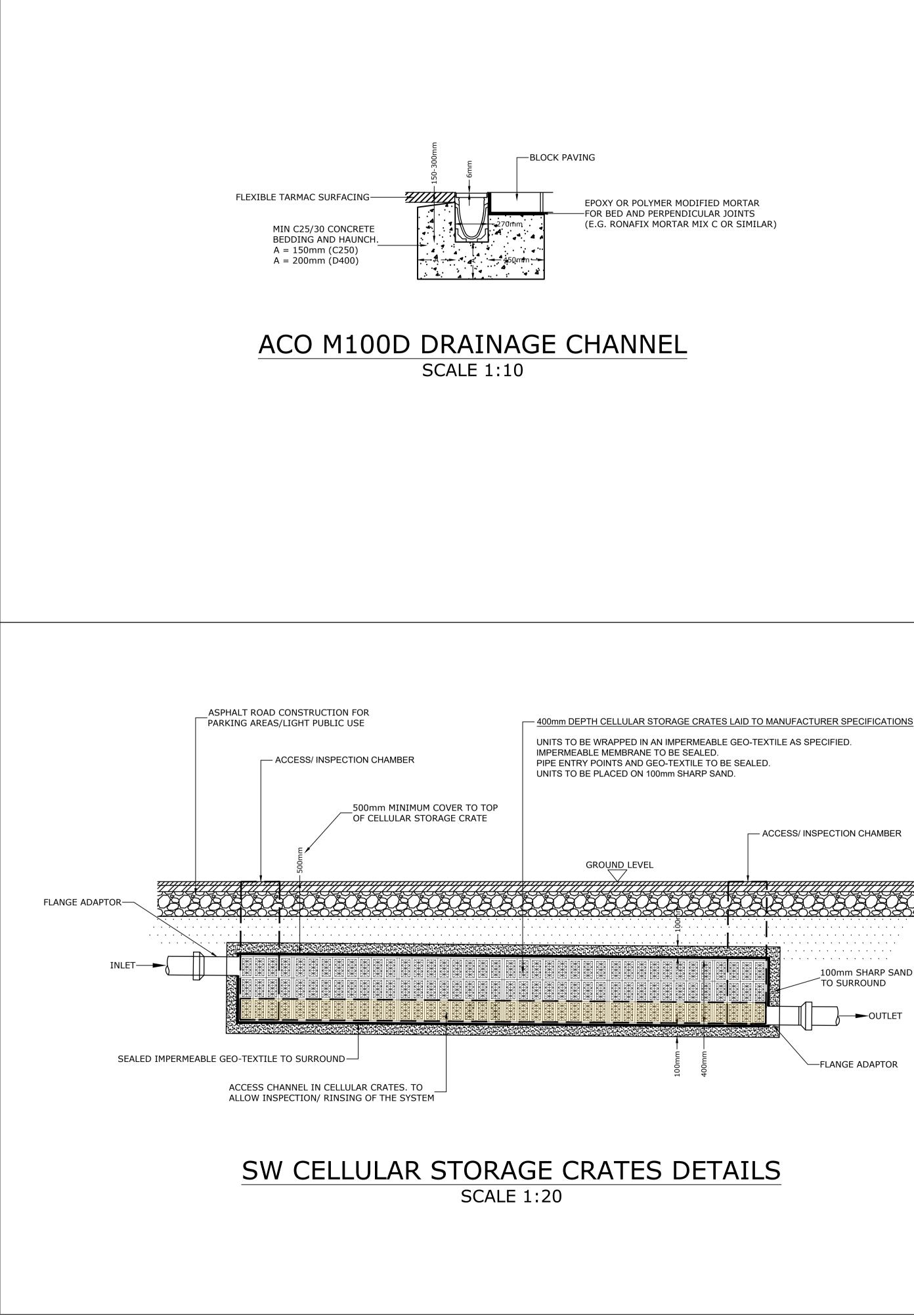
The traditional elements of the drainage system, as well as the SuDS will require maintenance. The owners of the properties will be tasked with the maintenance of the proposed drainage system and SuDS.

This maintenance agreement should include a detailed maintenance and management plan which expands on the above maintenance strategy, which should include all of the manufacturer specific maintenance requirements.

Attached

- Detailed Drainage Layout Plan
- Maintenance Schedules
- Detailed Drainage Drawings

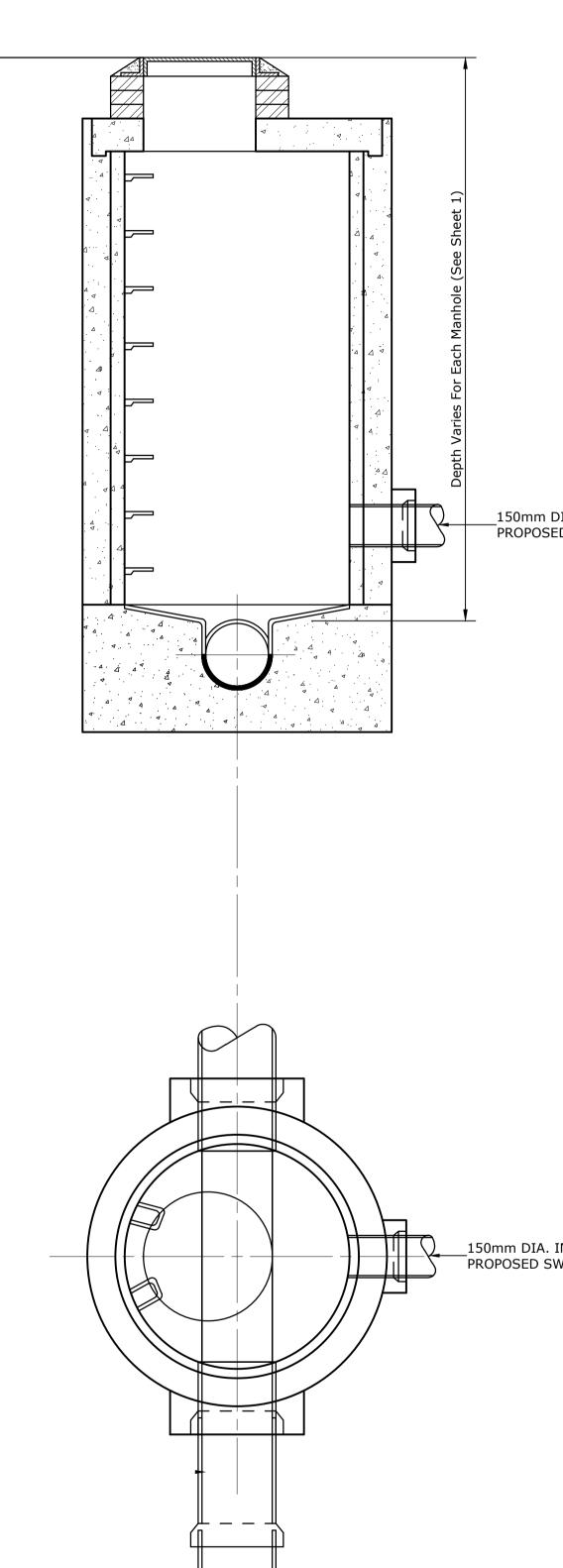




- ACCESS/ INSPECTION CHAMBER

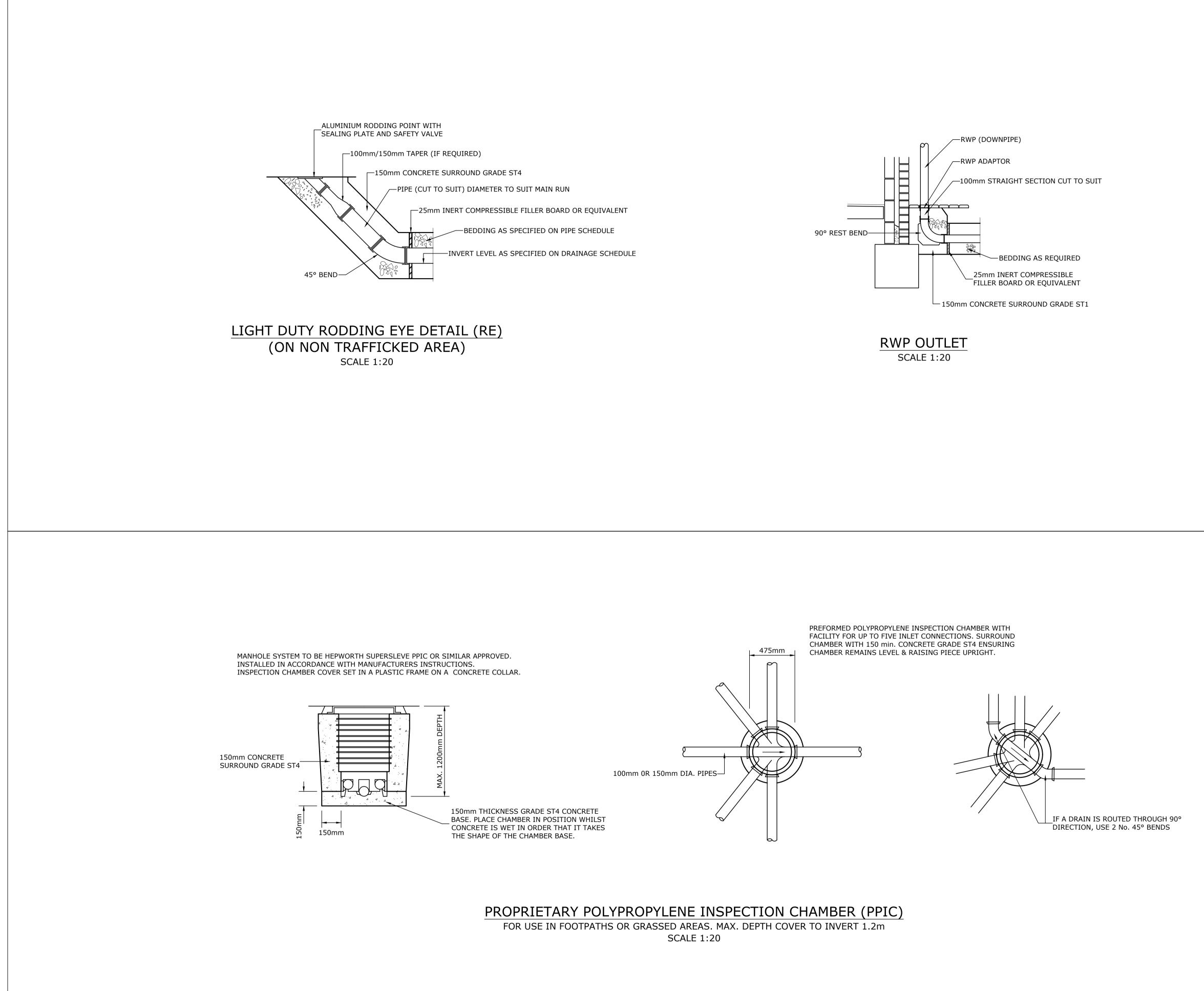
. 100mm SHARP SAND TO SURROUND

-FLANGE ADAPTOR



CONNECTION IN TO EXISTING SOUTHERN WATER MANHOLE SCALE 1:20

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Operation and Maintenance Schedule – Geo-Cellular Storage System						
Maintenance Schedule	Required Action	Typical Frequency				
	Inspect and identify any areas that are not operating correctly. If required, take remedial action.	Monthly for 3 months then annually				
Regular maintenance	Remove debris and sediment from the catchment surface, wherever is presents a risk to the performance of the drainage system,	Monthly, or as required based on inspection frequencies.				
	Remove sediment from pre-treatment structurers (e.g. sediment traps) and from internal forebays	Annually or as required based on inspection frequencies				
Remedial Actions	Repair; inlets, outlets, overflow pipes, and vent mechanisms	As required, based on inspections				
	Replace tank or geotextile if significant damage is observed or geotextile is torn.	As required				
	Inspect and check all inlets, outlets, vents, and overflows to ensure that they are in good condition and operating as designed.	Following installation, and annually hereafter				
Monitoring	Survey inside of tank, and at any sediment trap mechanisms, for sediment build-up and remove sediment if necessary. Use inspections to develop a regular maintenance and inspection procedure for sediment removal.	Every 5 years, or as required if inspections show high siltation rates.				

General Operation and Maintenance Table for Geo-Cellular Storage Systems

ACO Water Management: Building + Landscape

ACO RainDrain® B 125

- Ideal for driveways and light duty applications
- Easy and quick to install
- Clip locking grating for secure installation
- Full range of accessories for professional installation
- CE marked and fully certified to Load Class B 125 BS EN 1433:2002





ACO RainDrain® B 125

The ideal drainage channel for light duty applications

Manufactured from Vienite[®], ACO's high strength recycled polymer concrete material, ACO RainDrain[®] B 125 is suitable for vehicle traffic up to Load Class B 125.

The high quality ACO RainDrain $^{\otimes}$ B 125 channels interlock, allowing for quick and easy installation.

The channel comes complete with a cast iron Heelguard $^{\rm \tiny M}$ ATec grating making it ideal for driveway applications.

A full range of accessories are available, designed to aid simple and fast installation.

Applications

- Driveways
- Small private car parks
- Garage thresholds



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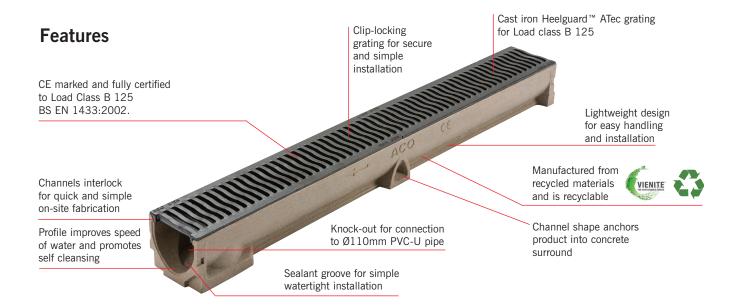


ACO RainDrain® B 125

System Overview



Driveways and small private car parks



ACO RAINDRAIN® B 125 ACCESSORIES

end cap



silt bucket





Ø110mm outlet end cap horizontal



Ø110mm drain union foul air-trap

ACO RainDrain® B 125 channel assembly

Product code	Description	Length (mm)	Width (mm)	Depth (mm)	Invert (mm)	Weight (kg)
47001	Channel with cast iron Heelguard™ ATec grating 1m	1000	118	97	87	10.97

ACO RainDrain® B 125 accessories

Product code	Description	Length (mm)	Width (mm)	Depth (mm)	Invert (mm)	Weight (kg)
20400	Cast iron Heelguard™ ATec grating 500mm B 125 *	500	118	15	-	2.45
47006	Sump with cast iron 47006 Heelguard™ ATec grating c/w slit bucket		118	303	275	13.60
319288	Closing end cap Ø110mm	6	129	97	-	0.03
319289	Outlet end cap	-	129	135	-	0.07
01684	Horizontal foul air trap	100	Ø110	-	-	0.20
0056	820 Drain union PVC-U Ø110mm	100	Ø110	-	-	0.10
1367	Lifting tools 5mm slots	-	-	-	-	0.20
2618	Socket plug UVPC Ø110mm	110	110	42	-	0.12

ACO RAINDRAIN® B 125 INSTALLATION



Dig trench 318mm wide (218mm wide if against a structure) by 200mm deep for channel (400mm deep for sump). Mark finishing height with fixed line 3mm below final surface. Lay 100mm (min.) bed of concrete



Lay channels starting from outlet/sump, ensuring joints connect by lowering units horizontally. Fit endcap to end channel. For fully watertight joints, use a suitable sealant (contact ACO for further advice).



Knock out pre-formed outlet from the inside (marked with hammer symbol) or fit sump or outlet endcap. Position sump or outlet channel on concrete bed, fit PVC-U union/trap to drainage pipework.



With gratings fitted, haunch around channels/sumps with concrete (suitable fill material). Final surface to be 3mm above grating. Bricks/paviours should be laid in mortar for lateral stability.



ACO Technologies plc ACO Business Park, Hitchin Road, Shefford, Bedfordshire SG17 5TE Tel: 01462 816666 Fax: 01462 815895 e-mail: technologies@aco.co.uk website: www.aco.co.uk

Polystorm Access

PRODUCT INFORMATION

Polystorm Access provides a 1m x 0.5m shaft within a Polystorm geocellular structure to enable surface access for remote camera inspection and maintenance activities, such as flushing and rodding.

The system consists of a 500mm diameter shaft which extends from surface level to the top of a Polystorm structure, at which point a turret provides an interface between the shaft and the inspection chamber within the Polystorm structure. At the bottom of the chamber, a base unit interlocks with the surrounding layer of Polystorm cells whilst supporting the geomembrane. A 350mm reduced access shaft cap is provided to comply with inspection chamber regulations.

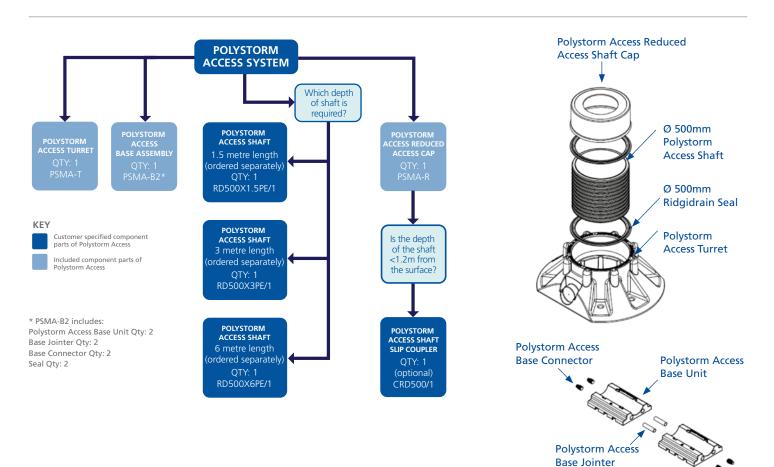
Polystorm Access is suitable for use with Polystorm, Polystorm-R, Polystorm Lite and Polystorm Xtra and may be combined with Polystorm Inspect for full length remote inspection and maintenance.



Please note: The Polystorm Access turret and base assembly are black. They are shown blue for illustration purposes.

Key Benefits

- Meets minimum 450mm width requirement for inspection chamber access, with 350mm reduced access where regulations dictate
- Integrated solution; can be used with Polystorm Inspect to monitor internal volume of geocellular structure
- Base unit provides smooth transition between Polystorm Inspect units
- Multiple inspection configurations can be achieved when used in conjunction with Polystorm Inspect
- Manufactured from polyethylene for light weight, ease of handling and high strength
- Sustainability: All components 100% recyclable after use



Polypipe Civils,

Charnwood Business Park, Loughborough, Leicestershire LE11 1LE Tel: +44 (0) 1509 615100 Fax: +44 (0) 1509 610215 Email: civils@polypipe.com www.polypipe.com/civils

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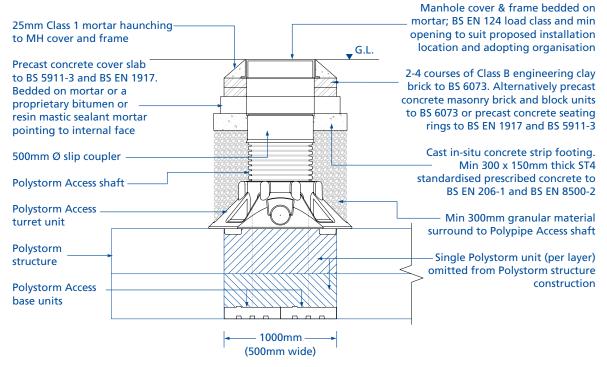
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P1 ISSUE 3 - JAN 2016

Polystorm Access

PRODUCT INFORMATION

Typical Elevation



Please note: Above is a typical installation detail for a Polystorm tank with groundwater below the base of the unit. For installation with groundwater above the structure invert please contact our Technical Team on +44 (0) 1509 615100 or email civils@polypipe.com

Polypipe Plastics Expertise

Polystorm Access is manufactured from sustainable polyethylene using the proven rotational moulding technique.

Reliability and Performance

All components in the Polystorm Access system have a design life of up to 50 years where ground conditions allow.

Easy Handling and Installation

Components are light and easy to handle, reducing health and safety risks and speeding up installation. The Polystorm Access shaft can be quickly and accurately cut to the right depth from 500mm Ridgidrain pipe, adding to the ease and flexibility on-site.

Nominal Weights

PSMA-B2 = 8kg PSMA-T = 19kg PSMA-R = 4kg

Flexible Positioning

The Polystorm Access turret can be positioned anywhere on a Polystorm structure, providing there are two or more Polystorm cells between the access turret and the structure edge. The Polystorm Access shaft is variable in length depending on the depth you require.

Features

- 1m x 0.5m inspection chamber within Polystorm structure
- 500mm riser shaft from surface to top of Polystorm structure
- Riser shaft may be extended as required using 500mm Ridgidrain pipe and seals
- It is recommended that the 500mm Ridgidrain pipe access shaft is within the limits of 250-1050mm for a standard installation
- Reduced Access shaft cap (350mm) available where required by regulations
- Utilises existing Polystorm Clips and Shear Connections
- Base unit manufactured from recyclable polyethylene
- Choice of standard shaft lengths

Technical Support

Detailed guidance and assistance is available. For further information, please contact our Technical Team on +44 (0) 1509 615100 or email civils@polypipe.com

All descriptions and illustrations in this publication are intended for guidance only and shall not constitute a 'sale by description'. All dimensions given are nominal and Polypipe may modify and change the information, products and specifications from time to time for a variety of reasons, without prior notice. The information in this publication is provided 'as is' on January 2016. Updates will not be issued automatically. This information is not intended to have any legal effect, whether by way of advice, representation or warranty (express or implied). We accept no liability whatsoever (to the extent permitted by law) if you place any reliance on this publication you must do so at your own risk. All rights reserved. Copyright in this publication belongs to Polypipe and all such copyright may not be used, sold, copied or reproduced in whole or part in any manner in any media to any person without prior consent. **Polypipe** is a registered trademark of Polypipe. All Polypipe products are protected by Design Right under CDPA 1988. Copyright © 2016 Polypipe. All rights reserved.

Polypipe Civils,

Charnwood Business Park, Loughborough, Leicestershire LE11 1LE Tel: +44 (0) 1509 615100 Fax: +44 (0) 1509 610215 Email: civils@polypipe.com www.polypipe.com/civils

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Data Sheet

ISSUE 3 - JAN 2016

P2

Polystorm Inspect

PRODUCT INFORMATION

Product code: PSM4

The Polystorm Inspect cell is complementary to the Polystorm range of modular cell solutions. Its primary purpose is to provide a tunnel along the length of a fully installed Polystorm structure to enable access for inspection and maintenance. Polystorm Inspect is a high strength thermoplastic cell which evenly distributes its load through the Polystorm structure. The tunnel end is left open by default but the unit can be closed off if required by clipping into place the moulded end plate. For purposes of identification the cell features a yellow centre section and end plate.



Ρ1

Key Benefits

- Creates a horizontal tunnel running through the middle of the tank to provide access for inspection and maintenance, i.e. jetting and rodding
- Can be used with Polystorm Lite, Polystorm-R and Polystorm (cannot be used in the same layer as Polystorm Xtra as the Polystorm Inspect cell is deeper)
- Tunnel can be used as a flow inlet track achieving greater stormwater flow distribution within the unit
- Large access tunnel (height 320mm and width 172mm nominal) – allows maximum field of vision while maintaining the system's structural performance
- High strength to weight ratio
- Light weight cell allows easier handling and reduced Health and Safety risk
- Utilises the same Shear Connectors and Clips as the Polystorm range
- The tunnel restricts the dissipation of silt in to the overall structure making inspection and maintenance easier
- Polystorm Inspect cells with 225mm (PSM4CRD225) or 300mm (PSM4CRD300) inlets are available

Applications

Polystorm Inspect is designed to work with the rest of the Polystorm range within a layered hybrid system enabling an intelligently engineered attenuation or infiltration structure to be created. It is intended to be used from the inlet point of the Polystorm structure. If used other than along an inlet tract, the Polystorm Inspect end plate should be used to cap off the tunnel entrance. The most cost effective way to create a tank is to use a combination of Polystorm Inspect cells and other Polystorm modular cells.

UNIT TYPE PHYSICAL PROPERTIES 1m Length Width 0.5m Depth 0.4m Total volume 0.2m³ Unit weight 11.6kg* 0.188m³ (188 litres) Cube storage volume 94% Volumetric void ratio SHORT TERM COMPRESSIVE STRENGTH Vertical Minimum 440kN/m² Lateral Minimum 63kN/m² SHORT TERM DEFLECTION Short-term vertical deflection Minimum 70.1kN/m² LONG TERM DEFLECTION 0.6113I.n Estimated long term vertical deflection (design life in hrs) (creep)

Note: The table above is applicable to PSM4 without the end plate. *Approximate weight

End plates to be purchased separately as required.

Please note: The use of Polystorm Inspect does not negate the requirement for a Silt Trap to be installed prior to the Polystorm structure. The use of a Silt Trap or other silt prevention device would always be recommended.

Technical Support

Detailed guidance and assistance is available. For further information, please contact our Technical Team on +44 (0) 1509 615100 or email civils@polypipe.com

Polypipe Civils

www.polypipe.com/wms

Charnwood Business Park, Loughborough, Leicestershire LE11 1LE Tel: +44 (0) 1509 615100 Fax: +44 (0) 1509 610215 Email: civils@polypipe.com



Data Sheet

ISSUE 2 - JAN 2016

Polystorm Inspect

PRODUCT INFORMATION

Data Sheet

ISSUE 2 - JAN 201

P2

RECOMMENDED MAXIMUM DEPTH OF INSTALLATION (to cell invert) [m]								
TYPICAL SOIL TYPE	TYPICAL ANGLE OF SHEAR RESISTANCE	(below ba	ROUNDWATER ase of cells) AL CASE	WITH GROUNDWATER AT 1M BELOW GROUND LEVEL AND UNITS WRAPPED IN GEOMEMBRANE				
		Pedestrian	Trafficked (cars)	Pedestrian	Trafficked (cars)			
Stiff over consolidated clay e.g. London clay	24°	2.3	2.0	1.8	1.7			
Normally consolidated silty sandy clay e.g. alluvium, made ground	26°	2.4	2.2	1.9	1.7			
Loose sand and gravel	30°	2.8	2.6	2.0	1.8			
Medium dense sand and gravel	33°	3.2	2.9	2.1	1.9			
Dense sand and gravel	38°	3.9	3.6	2.2	2.1			

Note:

1) Stated depths based on the calculation methodology detailed within CIRIA C680 (2008)

2) Assuming a soil density = 19 kN/m³ water density = 9.81 kN/m³

3) Assumed ultimate limit state (ULS) partial factor of safety applied to: Material = 2.75 Live load = 1.5 Dead load = 1.35

Notes:

- 1. Unless stated, all values are nominal and may vary within normal production tolerances.
- 2. Polypipe reserve the right to change product specifications without prior notice.
- 3. This document is uncontrolled and updates will not be issued automatically.

RECOMMENDED MINIMUM COVER LEVELS [m]							
LIVE LOAD CONDITIONS PEDESTRIAN LIGHT TRAFFICKED							
		Car park with vehicle mass <6000kg					
Minimum cover depth required (m)	0.50	0.60					

Note:

1) Stated depths based on the calculation methodology detailed within CIRIA C680 (2008)

2) Assumed serviceability limit state (SLS) partial factor of safety applied to: Material = 1.5 Live load = 1.0 Dead load = 1.0

3) Shallower minimum burial depths may be applicable subject to specific site conditions.

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Polypipe Civils

Charnwood Business Park, Loughborough, Leicestershire LE11 1LE Tel: +44 (0) 1509 615100 Fax: +44 (0) 1509 610215 Email: civils@polypipe.com



Polystorm-R Modular Cell

PRODUCT INFORMATION

Product code: PSM1A

The Polystorm-R modular cell is ideally suited for loaded applications at greater depths, such as housing, commercial and infrastructure projects and has a compressive strength of up to 61 tonnes/m². It offers all the proven performance of the Polystorm cell, with the added benefits of being manufactured from over 90% recycled material content.

Wherever performance criteria and standards allow, we will always maximise the sustainability of our products by using post consumer plastics in their manufacture. By sourcing and carefully controlling the quality of the recycled material we use our precision injection moulding. Therefore we are able to guarantee consistent quality in our recycled plastic, giving you the confidence and the performance levels you expect from the market leader.



Ρ1

Key Benefits

- Made from specially selected and controlled recycled materials
- Environmentally friendly, sustainable solution
- Has undergone stringent testing to ensure product performance
- Compressive strength of 61 tonnes/m²
- Ideal for retention, attenuation and infiltration applications with a suitable geomembrane or geotextile
- BBA approved
- Allow flexibility of shape ideal for shallow excavation systems, narrow strips or use in restricted areas
- Can be used as part of a value engineered hybrid system with Polystorm, Polystorm Lite and Polystorm Xtra
- Integrated inlet and outlet
- 3D flow throughout the structure
- 95% void ratio
- Light weight yet robust excellent Health and Safety and installation benefits
- 60 years creep limited life expectancy

Technical Support

Detailed guidance and assistance is available. For further information, please contact our Technical Team on +44 (0) 1509 615100 or email civils@polypipe.com



ELEMENT	VALUE
PHYSICAL PROPERTIES	
Length	1m
Width	0.5m
Depth	0.4m
Total volume	0.2m³
Unit weight	9kg (approx)
Unit storage volume	0.19m ³ (190 litres)
Void ratio	95%
SHORT TERM COMPRESSIVE STRENGTH	
Vertical	610 kN/m² **
Lateral	63 kN/m² **
SHORT TERM DEFLECTION	
Short-term vertical deflection	60 kN/m² per mm
LONG TERM DEFLECTION	
Estimated long term vertical deflection (creep)	0.2798 Ln (design life in hrs) +0.485 [Based on an applied test load = 162 kN/m ²] Creep data limit 60 years
Estimated long term lateral deflection (creep)	1.0192 Ln (design life in hrs) -3.864 [Based on an applied test load = 30.8 kN/m ²] Creep data limit 60 years

Note: Polystorm-R is ideal for use in trafficked and pedestrian applications subject to a structural design check and suitable installation conditions

* Each unit includes 4 Clips and 2 Shear Connectors.

** Compressive strength at yield, maximum recommended value for design purposes.

Polypipe Civils Charnwood Business Park, Loughborough, Leicestershire LE11 1LE Tel: +44 (0) 1509 615100 Fax: +44 (0) 1509 610215 Email: civils@polypipe.com

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ISSUE 4 - SEPT 2017

Polystorm-R Modular Cell

PRODUCT INFORMATION

RECOMMENDED MAXIMUM DEPTH OF INSTALLATION (to cell invert) [m]

TYPICAL SOIL TYPE	TYPICAL ANGLE OF SHEAR	SOIL WEIGHT	(below b	ROUNDWATER pase of cells) IAL CASE	WITH GROUNDWATER AT 1M BELOW GROUND LEVEL AND UNITS WRAPPED IN GEOMEMBRANE		
	RESISTANCE	kN/m³	Pedestrian	Trafficked (cars) <3000kg GVW	Pedestrian	Trafficked (cars) <3000kg GVW	
Stiff over consolidated clay e.g. London clay	24	20.0	2.2	1.9	1.8	1.6	
Normally consolidated silty sandy clay e.g. alluvium, made ground	26	19.0	2.4	2.2	1.9	1.7	
Loose sand and gravel	30	18.0	3.0	2.7	2.0	1.9	
Medium dense sand and gravel	33	19.0	3.2	2.9	2.0	1.9	
Dense sand and gravel	38	20.0	3.7	3.5	2.1	2.0	

Note:

1) Stated depths based on the calculation methodology detailed within CIRIA C680 (2008)

2) Assuming water density = 10.0kN/m³

3) Assumed ultimate limit state (ULS) partial factor of safety applied to: Material = 2.75 Lateral pressure = 1.35

Durability

The polymer material used in the manufacture of the Polystorm-R unit has an adequate resistance to attack from the type and quantities of chemicals that may be expected to naturally occur in uncontaminated soils and rainwater runoff. When installed in accordance with our recommendations, it is expected that the Polystorm-R unit will have a design life in excess of 60 years*. The installer of a proposed geocellular structure should ensure that an appropriate design check has been undertaken, in accordance with the recommended methodology and factors of safety given in CIRIA C680 (2008), Structural Design of Modular Geocellular Drainage Tanks, prior to the commencement of construction activities.

* Derived from long term extrapolated creep testing

Notes

- 1. Unless stated, all values are nominal and may vary within normal production tolerances.
- 2. The characteristic unit parameters stated have been based on Polypipe BBA certificate N° 06/4297, sheet 3.
- 3. Polypipe reserve the right to change product specifications without prior notice.
- 4. This document is uncontrolled and updates will not be issued automatically.

RECOMMENDED MINIMUM COVER LEVELS [m]						
LIVE LOAD PEDESTRIAN LIGHT TRAFFICKED						
		Car park with vehicle mass <gvw< td=""></gvw<>				
Minimum cover depth required (m)	0.50	<3000kg 0.50	<9000kg 0.65			

Note

1) Stated depths based on the calculation methodology detailed within CIRIA C680 (2008)

2) Assumed serviceability limit state (SLS) partial factor of safety applied to: Material = 1.5 Live load = 1.0 Dead load = 1.0

 Shallower minimum burial depths may be applicable subject to an assessment of the specific site conditions. For further details please consult our Technical Team on 01509 615100.

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Polypipe Civils

Charnwood Business Park, Loughborough, Leicestershire LE11 1LE Tel: +44 (0) 1509 615100 Fax: +44 (0) 1509 610215 Email: civils@polypipe.com www.polypipe.com/wms



ISSUE 4 - SEPT

P2

RIDGISTORMSeparate Catchpits

PRODUCT INFORMATION

RIDGISTORMSeparate Catchpits are designed to separate silt and other particles from stormwater, helping to protect the downstream drainage system and local environment. They can be integrated into our range of pipe systems, such as Ridgidrain and Ridgistorm-XL to offer a fully integrated drainage system.

Applications

RIDGISTORMSeparate Catchpits are pre-fabricated for use in a range of stormwater systems requiring silt and debris seperation and retention.

Key Features and Benefits

- Provides easy access for silt collection
- Network Rail Parts and Drawing System (PADs) approved for use in CESS Areas
- Separates silt and debris from the downstream drainage system
- Eliminates wastage associated with in-situ construction
- Multiple inlet and outlet options, supplied with integral sockets as standard allowing quick and seamless connection to pipeline
- Depths can be tailored to suit project requirements •
- Optional step rungs to BS EN 13101 and ladders to BS EN 14396
- Integral lifting points available on request to improve Health • and Safety of handling and installation
- Stub connections and rocker pipes are available

Other fabrications in our RIDGISTORMSeparate range:

- Silt Traps
- Filter Chambers

Performance

RIDGISTORMSeparate Catchpits are fabricated from Ridgistorm-XL pipework, which is manufactured to meet the material requirements of BS EN 13476:2007 (Part 1-3).

RIDGISTORMSEPARATE CATCHPITS

PHYSICAL PROPERTIES	
Diameter	450-3000mm
Depth	To suit requirements
Sump depth	To suit (min. 50mm)
Material	HDPE
Colour	Black with blue Interior
Chemical resistance	HDPE is naturally resistant to most chemicals associated with stormwater drainage systems
Inlets/outlets	100-3000mm

Our Ridgistorm-XL Fabrications range

All of our Ridgistorm-XL fabrications are tailor-made, fully-welded, watertight structured wall chambers to suit project-specific requirements. Health and Safety benefits become apparent during handling and installation, due to our fabrications' strong but light in weight nature. In addition, off-site construction ensures uncompromised, high quality products being delivered to site ready-to-install, reducing installation time and costs.



Data Sheet

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Ρ1



Polypipe

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Charnwood Business Park, Loughborough, Leicestershire LE11 1LE Tel: +44 (0)1509 615100 Fax: +44 (0)1509 610215 Email: civils@polypipe.com

RIDGISTORMSeparate Catchpits

RIDGISTORMSeparate Chamber Wall

> (size and orientation

PRODUCT INFORMATION

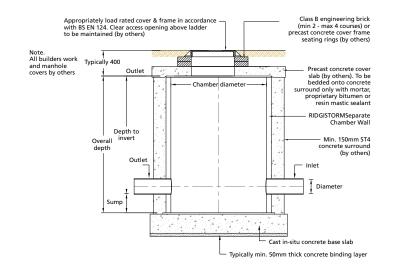
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RIDGISTORMSeparate Catchpit

Min 0450

Outlet — (size and orientation as required



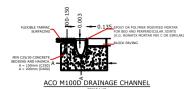


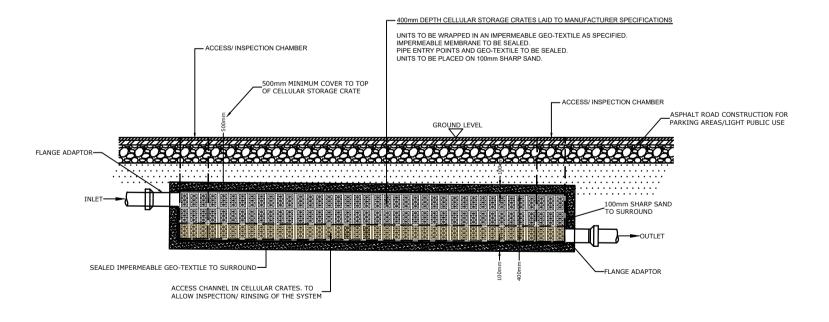
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Charnwood Business Park, Loughborough, Leicestershire LE11 1LE Tel: +44 (0)1509 615100 Fax: +44 (0)1509 610215 Email: civils@polypipe.com www.polypipe.com/civils







SW CELLULAR STORAGE CRATES DETAILS

SCALE 1:20





Herrington Consulting Ltd Units 6 & 7 Barham Business Park Elham Valley Road Canterbury Kent CT4 6DQ Your ref

Our ref DS_CC_PDE-119744 Date 07 October 2020 Contact Tel 0330 303 0119

Dear Sir/Madam,

Level 1 Capacity Check Enquiry: 53 Joy Lane, Whitstable, Kent, CT5 4DB.

We have completed the capacity check for the above development site and the results are as follows:

Foul Water

There is currently adequate capacity in the local sewerage network to accommodate a foul flow of **0.03 I/s** for the above development at manhole reference TR0965**9502**. Please note that no surface water flows (existing or proposed) can be accommodated within the existing foul sewerage system unless agreed by the Lead Local Flood Authority in consultation with Southern Water, after the hierarchy Part H3 of Building Regulations has been complied with.

Surface Water

There is currently adequate capacity in the local surface water network to accommodate a surface water flow of **2.1 I/s** for the above development at manhole reference TR0965**9550**.

Although capacity in the surface water network has been identified, in all situations where surface water is being considered for discharge to our network, we require the below hierarchy for surface water to be followed which is reflected in part H3 of the Building Regulations. Whilst reuse does not strictly form part of this hierarchy, Southern Water would encourage the consideration of reuse for new developments.

Southern Water Services Ltd, Registered Office: Southern House, Yeoman Road, Worthing West Sussex BN13 3NX Registered in England No. 2366670

Ise	Consider	ion	Consider	d V	Consider	Ver	Consider	Ver	Consider
Reu	Rain harvesting reduces demand on water supply and quantity of runoff discharged from site.	Infiltration	Infiltration potential, even if infiltration rates are low to reduce the volume of runoff from sites.	Watercourse	High flow conditions. Requirements for Consent to discharge.	Storm sev	Existing capacity of the sewer. Potential for surcharge conditions within the sewer at time of discharge.	Combined sev	the combined sewer should not increase the risk of

Guidance on Building Regulations is here: <u>gov.uk/government/publications/drainage-and-waste-</u> <u>disposal-approved-document-h</u>

We would welcome the opportunity to engage with you on the design for disposal of surface water, with a particular focus on the potential for incorporating Sustainable Drainage Systems (SuDS), for this development at the earliest opportunity and we recommend that civil engineers and landscape architects work together and with Southern Water.

Where a surface water connection to the foul or combined sewer is being considered, this should be agreed by the Lead Local Flood Authority, in consultation with Southern Water.

It should be noted that although the above assessment indicates that there is capacity available for your proposed surface water flows the LLFA (Local Lead Flood Authority) may impose/request that a lower flow is discharged to the public surface water sewer.

If the excess surface water flows are to be attenuated on site, it could have a significant effect on any proposed Sewer Adoption (S104) Agreements. Any attenuation proposals should be agreed before any works are implemented on site. Where capacity is limited/restricted, agreement should be sought if you are to include any highway drainage within your proposals as Southern Water is not obligated to accept highway flows.

Connecting to our network

It should be noted that this information is only a hydraulic assessment of the existing sewerage network and does not grant approval for a connection to the public sewerage system. A formal Sewer Connection (S106) application is required to be completed and approved by Southern Water Services. To make an application visit: <u>developerservices.southernwater.co.uk/</u>

Please note the information provided above does not grant approval for any designs/drawings submitted for the capacity analysis. The results quoted above are only valid for 12 months from the date of issue of this letter.

Southern Water, Southern House, Yeoman Road, Worthing, West Sussex, BN13 3NX southernwater.co.uk

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Should it be necessary to contact us please quote our above reference number relating to this application by email at <u>southernwaterplanning@southernwater.co.uk</u>

Yours sincerely,

The

Joff Edevane Growth Planning Lead **Business Channels**

SOUTHERN WATER

