



KNAPP HICKS & PARTNERS LTD

CONSULTING STRUCTURAL, CIVIL & GEOTECHNICAL ENGINEERS



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Knapp Hicks & Partners Ltd

Incorporated in England
No. 2886020

Registered office:

Laval House

SURFACE WATER DRAINAGE DESIGN


ADDENDIUM TO 34109/R004/AJB

HOWE BARRACKS

April 2018
34109/R004/AJB

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Phase 1, 1 in 100 Year Calculation
Infiltration Test Results

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Date 23/05/2018 16:58	Designed by AJB	
File PHASE 1 SW REV.MDX	Checked by	
Causeway	Network 2015.1	

Summary of Critical Results by Maximum Level (Rank 1) for Storm

Simulation Criteria

Areal Reduction Factor 1.000 Additional Flow - % of Total Flow 0.000
Hot Start (mins) 0 MADD Factor * 10m³/ha Storage 2.000
Hot Start Level (mm) 0 Inlet Coefficient 0.800
Manhole Headloss Coeff (Global) 0.500 Flow per Person per Day (l/per/day) 0.000
Foul Sewage per hectare (l/s) 0.000

Number of Input Hydrographs 0 Number of Offline Controls 0 Number of Time/Area Diagrams 0
Number of Online Controls 8 Number of Storage Structures 0 Number of Real Time Controls 0


Synthetic Rainfall Details

Rainfall Model FSR Ratio R 0.379
Region England and Wales Cv (Summer) 0.750
M5-60 (mm) 19.800 Cv (Winter) 0.840

Margin for Flood Risk Warning (mm) 300.0
Analysis Timestep 2.5 Second Increment (Extended)
DTS Status ON
DVD Status ON
Inertia Status ON

Profile(s) Summer and Winter
Duration(s) (mins) 15, 30, 60, 120, 180, 240, 360, 480, 600, 720,
960, 1440, 2160, 2880, 4320, 5760, 7200, 8640,
10080
Return Period(s) (years) 100
Climate Change (%) 20

PN	US/MH Name	Storm	Return Period	Climate Change	First (X) Surchage	First (Y) Flood	First (Z) Overflow	Overflow Act.	Water Level (m)
1.000	ASV2	60 Winter	100	+20%	100/15 Winter				50.281
1.001	ASV1	60 Winter	100	+20%	100/15 Summer				50.277
1.002	AS1	60 Winter	100	+20%	100/15 Summer				50.266
2.000	AS13	60 Winter	100	+20%	100/60 Winter				50.300
2.001	AS14	60 Winter	100	+20%	100/60 Winter				50.295
2.002	AS15	60 Winter	100	+20%	100/15 Summer				50.273
2.003	AS16	60 Winter	100	+20%	100/15 Winter				50.262
1.003	AS2	60 Winter	100	+20%	100/15 Summer				50.244
3.000	AS17	60 Winter	100	+20%	100/30 Summer				50.271
3.001	AS18	60 Winter	100	+20%	100/15 Winter				50.263
3.002	AS19	60 Winter	100	+20%	100/15 Summer				50.249
1.004	AS3	60 Winter	100	+20%	100/15 Summer				50.242
1.005	AS4	60 Winter	100	+20%	100/15 Summer				50.239
1.006	AS5	60 Winter	100	+20%	100/15 Summer				50.236
4.000	AS20	180 Winter	100	+20%	100/60 Winter				49.348
4.001	AS21	180 Winter	100	+20%	100/60 Winter				49.348
4.002	AS22	180 Winter	100	+20%	100/60 Winter				49.348
4.003	AS23	180 Winter	100	+20%	100/60 Summer				49.323
5.000	AS24	15 Winter	100	+20%					49.557
6.000	AS26	15 Winter	100	+20%					49.832
5.001	AS25	180 Winter	100	+20%					49.300

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Summary of Critical Results by Maximum Level (Rank 1) for Storm

PN	US/MH Name	Storm	Return Period	Climate Change	First (X) Surchage	First (Y) Flood	First (Z) Overflow	Overflow Act.	Water Level (m)	
1.007	AS6	180	Winter	100	+20%	100/30	Summer		49.300	
7.000	AS27	180	Winter	100	+20%	100/120	Summer		48.952	
1.008	AS7	180	Winter	100	+20%	100/15	Summer		48.952	
1.009	AS8	180	Winter	100	+20%	100/15	Winter		48.593	
1.010	AS9	180	Winter	100	+20%	100/30	Winter		48.212	
8.000	AS28	360	Winter	100	+20%	100/60	Summer		47.827	
9.000	AS30	360	Winter	100	+20%	100/60	Winter		47.827	
8.001	AS29	360	Winter	100	+20%	100/60	Summer	100/180	Winter	47.827
1.011	AS10	360	Winter	100	+20%	100/30	Summer	100/120	Winter	47.828
1.012	AS11	240	Winter	100	+20%	100/15	Summer	100/120	Winter	47.850
1.013	AS12	360	Winter	100	+20%	100/15	Summer	100/120	Winter	47.862

PN	US/MH Name	Surcharged		Flooded		Pipe		Level Exceeded
		Depth (m)	Volume (m ³)	Flow / Cap.	Overflow (l/s)	Flow (l/s)	Status	
1.007	AS6	1.225	0.000	0.01		27.6	SURCHARGED	
7.000	AS27	0.767	0.000	0.01		1.9	SURCHARGED	
1.008	AS7	2.092	0.000	0.01		16.5	SURCHARGED	
1.009	AS8	2.068	0.000	0.02		17.0	SURCHARGED	
1.010	AS9	1.927	0.000	0.01		17.3	SURCHARGED	
8.000	AS28	1.272	0.000	0.01		4.9	FLOOD RISK	
9.000	AS30	0.812	0.000	0.01		1.6	FLOOD RISK	
8.001	AS29	1.707	6.702	0.02		7.8	FLOOD	4
1.011	AS10	2.088	27.858	0.04		37.5	FLOOD	9
1.012	AS11	2.315	0.368	0.03		26.3	FLOOD	8
1.013	AS12	3.077	0.055	0.40		15.1	FLOOD	6



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Soakaway Test

Site Royal Parade
 Job No. 34109
 Borehole SS101

Trial Pit Dimensions Width Length Depth
 0.45 m 1.1 m 0.65 m

Filled Water Level 0.269 m

75% effective depth 0.36425 m

50% effective depth 0.4595 m

25% effective depth 0.55475 m

Soil type at test depth Made Ground

The infiltration rate (f) is given by;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

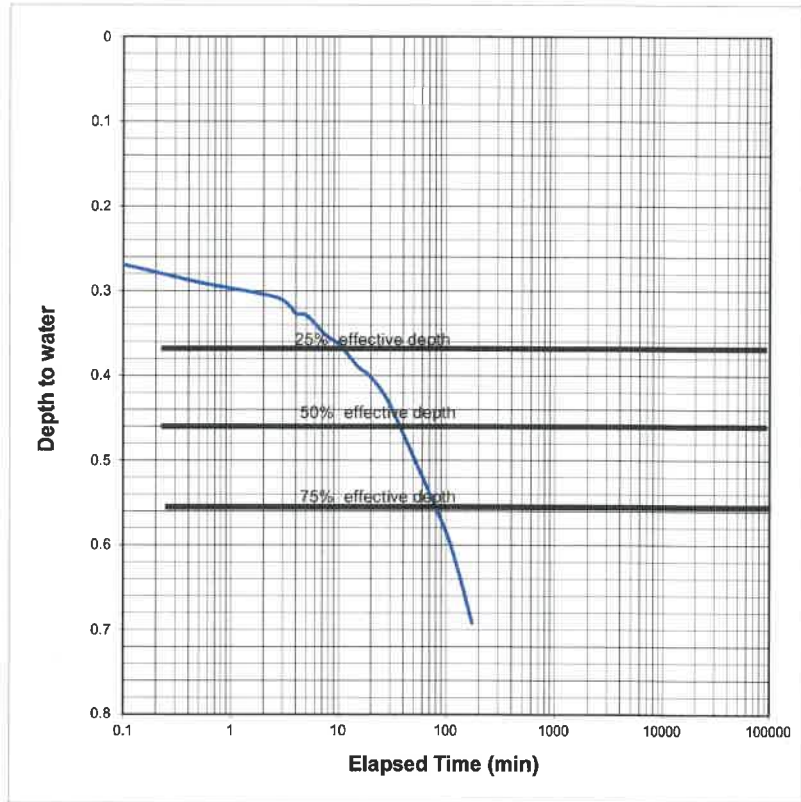
where:

V_{p75-25} = the effective storage volume of water in the trial pit between 75% and 25% effective depth

a_{p50} = the internal surface area of the trial pit up to 50% effective depth and including the base area

t_{p75-25} = the time for the water level to fall from 75% to 25% effective depth

Time (mins)	Depth m
0.1	0.269
0.5	0.29
1	0.297
1.5	0.301
2.5	0.307
3	0.311
3.5	0.318
4	0.327
5	0.329
7.5	0.352
10	0.363
15	0.389
20	0.402
30	0.435
92	0.573
123	0.62
174	0.692



$V_{p75-25} = 0.0942975 \text{ m}^3$ m^3

$a_{p50} = 1.08555 \text{ m}^2$

Infiltration factor

* $t_{p75-25} = 4200 \text{ seconds}$

$f = 2.06824\text{E-}05 \text{ ms}^{-1}$

Note;

* Indicates that the full drainage was not achieved within the duration of the test. Consequently, the infiltration value has been calculated using the reduced depth test as outlined in BRE 365. Caution should be applied to the value obtained and where possible further long term testing carried out.



Site Royal Parade
Job No. 34109
Borehole SS102

Trial Pit Dimensions Width Length Depth
 0.45 m 1.2 m 0.7 m

Filled Water Level 0.269 m

75% effective depth 0.37675 m

50% effective depth 0.4845 m

25% effective depth 0.59225 m

Soil type at test depth Made Ground

The infiltration rate (f) is given by;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

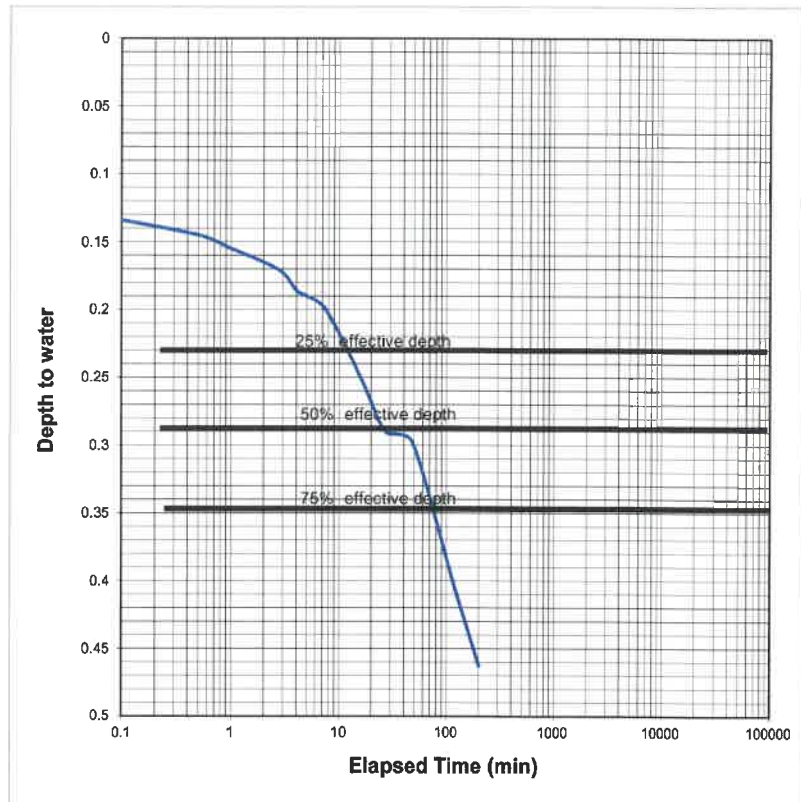
where:

V_{p75-25} = the effective storage volume of water in the trial pit between 75% and 25% effective depth

a_{p50} = the internal surface area of the trial pit up to 50% effective depth and including the base area

t_{p75-25} = the time for the water level to fall from 75% to 25% effective depth

Time (mins)	Depth m
0.1	0.134
0.5	0.145
1	0.155
2	0.165
3	0.173
4	0.186
5	0.19
7.5	0.2
16.5	0.253
27	0.29
48	0.298
119	0.405
201	0.463



V_{p75-25} = 0.11637 m³ m³

a_{p50} = 1.25115 m² Infiltration factor

* t_{p75-25} = 3900 seconds $f = 2.38488E-05 \text{ ms}^{-1}$

Note;

* Indicates that the full drainage was not achieved within the duration of the test. Consequently, the infiltration value has been calculated using the reduced depth test as outlined in BRE 365. Caution should be applied to the value obtained and where possible further long term testing carried out.



Site Royal Parade
Job No. 34109
Borehole SS103 Test 1

Trial Pit Dimensions Width Length Depth
 0.45 m 1.0 m 0.62 m

Filled Water Level 0.193 m

75% effective depth 0.29975 m

50% effective depth 0.4065 m

25% effective depth 0.51325 m

Soil type at test depth Made Ground

The infiltration rate (f) is given by;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

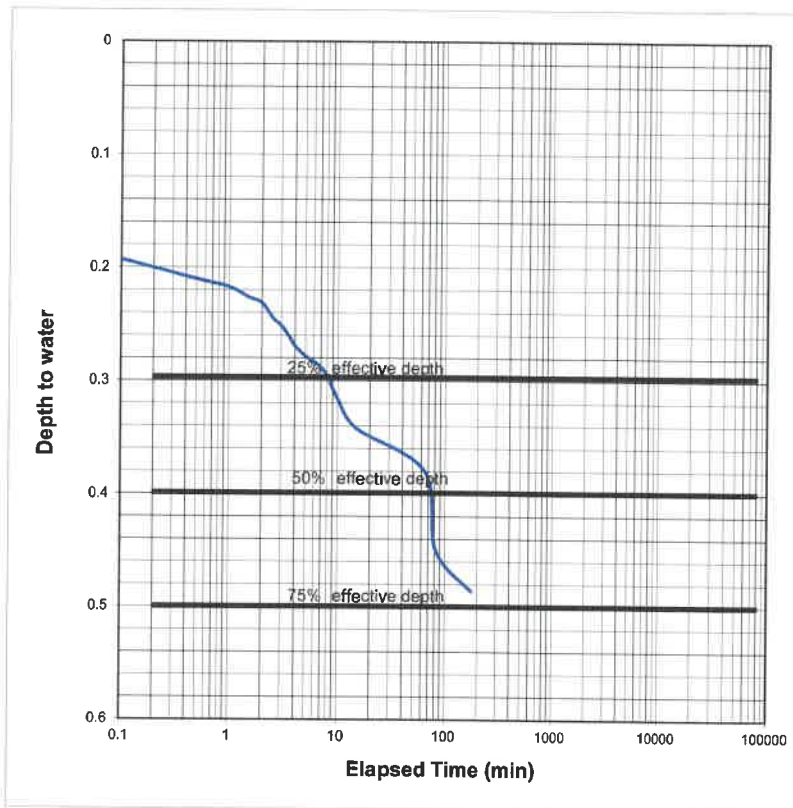
where:

V_{p75-25} = the effective storage volume of water in the trial pit between 75% and 25% effective depth

a_{p50} = the internal surface area of the trial pit up to 50% effective depth and including the base area

t_{p75-25} = the time for the water level to fall from 75% to 25% effective depth

Time (mins)	Depth (m)
0.1	0.193
0.5	0.21
1	0.217
1.5	0.226
2	0.231
2.5	0.244
3	0.251
3.5	0.26
4	0.269
5	0.278
7.5	0.291
10	0.316
15	0.342
65	0.38
82.5	0.45
178	0.486



$V_{p75-25} = 0.096075 \text{ m}^3$ m^3

$a_{p50} = 1.06915 \text{ m}^2$

Infiltration factor

* $t_{p75-25} = 8520 \text{ seconds}$

$f = 1.05471\text{E-}05 \text{ ms}^{-1}$

Note;

* Indicates that the full drainage was not achieved within the duration of the test. Consequently, the infiltration value has been calculated using the reduced depth test as outlined in BRE 365. Caution should be applied to the value obtained and where possible further long term testing carried out.



Site Royal Parade
Job No. 34109
Borehole SS103 Test 2

Trial Pit Dimensions	Width 0.45 m	Length 1.0 m	Depth 0.62 m
Filled Water Level	0.146 m		
75% effective depth	0.2645 m		
50% effective depth	0.383 m		
25% effective depth	0.5015 m		
Soil type at test depth	Made Ground		

The infiltration rate (f) is given by;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

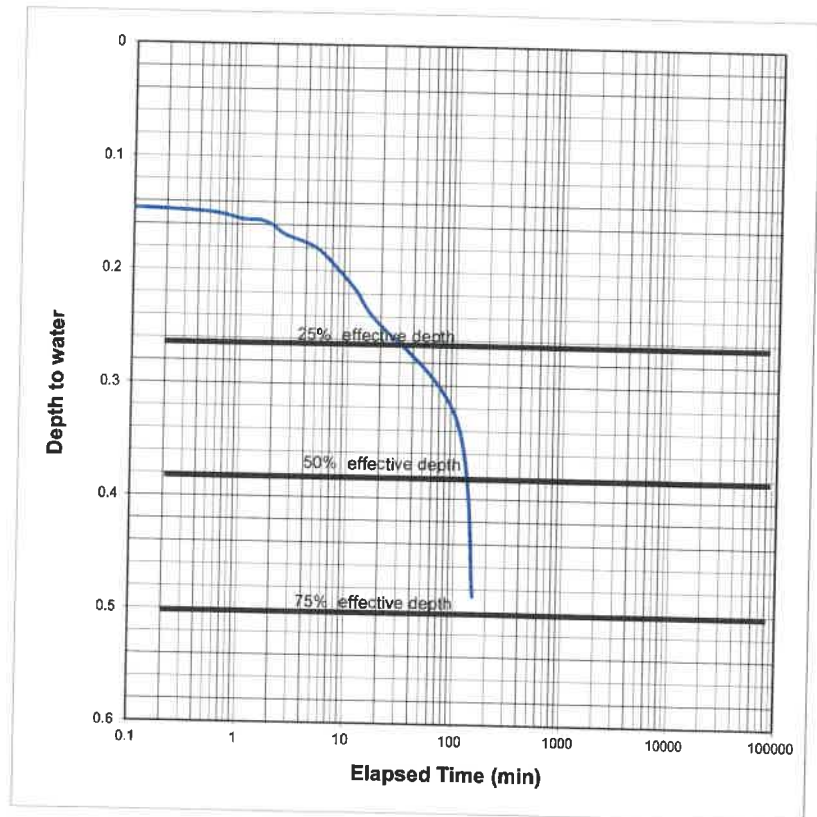
where:

V_{p75-25} = the effective storage volume of water in the trial pit between 75% and 25% effective depth

a_{p50} = the internal surface area of the trial pit up to 50% effective depth and including the base area

t_{p75-25} = the time for the water level to fall from 75% to 25% effective depth

Time (mins)	Depth m
0.1	0.146
0.5	0.149
1	0.155
1.5	0.156
2	0.161
2.5	0.168
5	0.18
8	0.199
12	0.219
16	0.238
100	0.328
150	0.486



$V_{p75-25} = 0.10665 \text{ m}^3$

$a_{p50} = 1.1373 \text{ m}^2$

Infiltration factor

* $t_{p75-25} = 8520 \text{ seconds}$

$f = 1.10064\text{E-}05 \text{ ms}^{-1}$

Note;

* Indicates that the full drainage was not achieved within the duration of the test. Consequently, the infiltration value has been calculated using the reduced depth test as outlined in BRE 365. Caution should be applied to the value obtained and where possible further long term testing carried out.