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KNAPP HICKS & PARTNERS LTD

CONSULTING STRUCTURAL, CIVIL & GEOTECHNICAL ENGINEERS



SURFACE WATER DRAINAGE DESIGN

HOWE BARRACKS

April 2018 34109/R004/AJB



SURFACE WATER DRAINAGE DESIGN FOR HOWE BARRACKS

| Report Status: DRAFT Date of Issue: April 2018 REV B | | | | | |
|--|---------------|--------------------|--|--|--|
| Name Signature & Date | | | | | |
| Author: | Andrew Bird | MBird 24.04.18 | | | |
| Checked & Approved: | Claire Taylor | CE Tayles 24/04/18 | | | |

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1 INTRODUCTION

This report details the proposed surface water drainage design for the development to the Howe Barracks development and has been written to address planning conditions for that site.

2 SITE DESCRIPTION

The site is located at NGR TR 16583 58162 to the East of Canterbury city centre. It is a brownfield site which has previously been used as a military barracks.

It is a roughly trapezoidal site with frontage onto Littlebourne Road and benefits from access onto Chaucer Road. The site is currently a partial brownfield site which covers a total area measuring 28 Ha.

The site has a gentle fall from east to west and from south to north but falls sharply through Chaucer Road and in the northwest corner near the proposed Legacy Park area.

3 EXISTING DRAINAGE

The sewer map for the locality shows surface and foul water sewers adjacent to the site in Littlebourne Road. It is believed that there is not capacity within the existing surface water sewer network to accept any additional flows. However, the existing development located within Howe barracks is estimated to contribute into the public surface water sewer with discharge rates estimated to be approximately 115L/s for the 1 in 30 year storm return period (see existing contributing area plan, Appendix A) and 145L/s for the 1 in 100 year storm return period

The developed site would cover an area of 13.8Ha with the additional land given over to park land and conservation areas; and this would have an estimated greenfield run-off rate of 27.3L/s.

The equivalent area based on Canterbury City Council's Brownfield run off rate, at a maximum of 4L/s/ha, would produce a peak controlled discharge rate site wide of approximately 55L/s which would be an improvement over the existing surface water sewer discharge. All existing and new connections would be subject to the agreement of Southern Water and will require a Section 106 agreement.

Proposals are for Phase 1 to discharge at a controlled 15L/s and for the remaining phases to discharge at a controlled rate of 40L/s and that the surface water sewers will be offered for adoption under a formal Section 106 agreement with Southern Water.

4 GEOLOGY & HYDROGEOLOGY

Following on from recent ground investigations, the prevailing ground conditions consist of a gravelly clay head deposits overlying fine sand with localised deposits of made ground.

Infiltration across the development has been found to be variable with results indicating that within the gravelly head deposits infiltration rates are medium to low but within the fine sand these are low to very low intrusive

Infiltration tests have revealed soakage rates of $1.6 \times 10^{-5} \text{m/s}$ within the gravely head deposits, and $1.00 \times 10^{-10} \text{m/s}$ within the fine sandy strata (see appendix A).

The site is set upon a minor aquifer and is located outside of an Environment Agency area defined Groundwater Source Protection Zone,

5 PROPOSED PHASE 1 DEVELOPMENT

For Phase 1 it is proposed to construct 171 dwellings with associated access roads and hardstanding areas.

It is proposed to discharge the majority of the surface water runoff generated by roof and private areas from this development to ground via a series of shallow soakaways into the gravely head deposits. A proportion of the residential surface water run-off will discharge into a new surface water sewer located in the carriageway. The new surface water sewer will be offered for adoption under a formal section 104 agreement with Southern water and will discharge to the existing public surface water in Littlebourne Road.

The proposed residential soakaways would be in the form of permeable paving located in private parking areas and forecourts.

The following table indicates depth of permeable sub-base required for a 1 in 100 year rainfall event plus 20% allowance for climate change. Allowing for a further additional 10% increase in area for urban sprawl, Sub-base depth have been standardised to allow for the maximum sub-base depth of 440mm. Additional volumes predicted during the 40% climate change event would be located within the sand and block courses with a slight possibility of minimal surface water flooding in a few locations. It is not believe that any surface water flows will be generated during the 1 in 100 year event plus 40% allowance for climate change. Finished floor levels have been set 150mm above finished ground levels and no flooding has been predicted

| | | RMEABLE AREA | | | |
|-------------------------|------------------------|-------------------------------------|--|---------------------------------|--------------|
| Plot Numbers | Contributing Area (m²) | Private Impermeable Area (m²) | Depth Of Sub- Base Required (mm) | Half drain time (minutes) | Urban Sprawl |
| 1-2 | 250 | 85 | 401 | 206 | 440 |
| 3-4 | 250 | 85 | 401 | 206 | 440 |
| 5-13 | 740 | 437 | 183 | 93 | 204 |
| 14-15 | 220 | 80 | 350 | 177 | 393 |
| 16-17 | 220 | 80 | 350 | 177 | 393 |
| 18-19 | 240 | 80 | 393 | 200 | 437 |
| 20-25 | 490 | 214 | 275 | 145 | 304 |
| 26-27 | 220 | 85 | 323 | 162 | 363 |
| 28-29 | 210 | 75 | 359 | 181 | 405 |
| 30-31 | 210 | 75 | 359 | 181 | 405 |
| 32 | 100 | 37 | 342 | 225 | 389 |
| 33 | 110 | 37 | 389 | 172 | 435 |
| 34 | 90 | 31 | 377 | 199 | 432 |
| 35 | 90 | 31 | 377 | 190 | 432 |
| 36 | 100 | 37 | 342 | 190 | 435 |
| 37 | 100 | 37 | 342 | 199 | 389 |
| 38-39 | 210 | 75 | 359 | 172 | 382 |
| 40-41 | 200 | 75 | 336 | 187 | 382 |
| 42-49 | 860 | 448 | 217 | 169 | 248 |
| 50-56 59-60 63-69 | 1410 | 595 | 319 | 160 | 363 |
| 54-56 | 260 | 85 | 401 | 212 | 440 |
| 57 | 110 | 38 | 375 | 172 | 430 |

| 58 | 110 | 38 | 375 | 172 | 430 |
|------------|-----|-----|-----|-----|-----|
| 61 | 110 | 38 | 375 | 212 | 430 |
| 62 | 110 | 38 | 375 | 212 | 430 |
| 63-65 | 260 | 85 | 403 | 112 | 440 |
| 70-77 | 690 | 224 | 407 | 208 | 440 |
| 78 | 90 | 38 | 287 | 153 | 330 |
| 79-81 | 170 | 64 | 334 | 167 | 415 |
| 82-86 & 93 | 820 | 400 | 237 | 123 | 268 |
| 87 | 180 | 82 | 260 | 136 | 298 |
| 88 | 130 | 46 | 326 | 164 | 363 |
| 89 | 170 | 71 | 291 | 153 | 338 |
| 90-93 | 570 | 500 | 177 | 89 | 190 |
| 94-95 | 160 | 70 | 274 | 144 | 320 |
| 96-97 | 230 | 78 | 384 | 195 | 429 |
| 98-99 | 230 | 78 | 384 | 195 | 429 |
| 100-101 | 220 | 78 | 362 | 184 | 407 |
| 102 | 130 | 46 | 326 | 180 | 363 |
| 103-104 | 260 | 95 | 348 | 176 | 392 |
| 105-106 | 260 | 95 | 348 | 176 | 392 |
| 107-108 | 260 | 95 | 348 | 176 | 392 |
| 109-110 | 240 | 80 | 393 | 200 | 437 |
| 111-113 | 220 | 87 | 313 | 167 | 352 |
| 114 | 85 | 30 | 281 | 169 | 336 |
| 115 | 110 | 42 | 328 | 175 | 369 |
| 116-117 | 210 | 80 | 329 | 166 | 372 |
| 118-120 | 320 | 106 | 397 | 202 | 435 |
| 121-125 | 480 | 230 | 243 | 127 | 270 |
| 126-128 | 460 | 243 | 213 | 110 | 238 |
| 129-130 | 240 | 95 | 312 | 167 | 348 |
| 131-132 | 200 | 77 | 324 | 163 | 369 |
| 136-137 | 380 | 240 | 163 | 90 | 187 |
| 138-139 | 220 | 79 | 356 | 180 | 400 |
| 140-141 | 250 | 106 | 285 | 151 | 306 |
| 142 | 110 | 46 | 326 | 172 | 363 |
| 143-144 | 200 | 69 | 376 | 191 | 426 |
| 145-148 | 400 | 182 | 260 | 136 | 294 |
| 149 | 110 | 40 | 339 | 200 | 375 |
| 150-153 | 700 | 352 | 228 | 118 | 258 |
| 155-158 | 430 | 207 | 242 | 126 | 271 |
| 159-171 | 840 | 404 | 242 | 126 | 271 |

Based on a infiltration rate of 1.6x10⁻⁵m/s

6 PUBLIC SURFACE WATER SEWERS

Highway drainage and a proportion of the residential drainage is proposed to flow into a Public Surface Water Sewer located within the adoptable highway and to discharge into the existing Public Surface Water Sewer in Littlebourne Road. Discharge would be controlled via a hydro brake to a maximum of 15 L/s.

Current design criteria for adoptable drainage is for the 1 in 30 year event plus 30% allowance for climate change. Windes calculations indicate that the current design complies with this storm event.

Discussions with Southern Water have been progressed and a verbal agreement has been reached on the surface water discharge from Phase 1 into Littlebourne Road. These are

currently being vetted by Southern Water with a view to offering the onsite drainage for adoption under a Section 104 agreement.

Projecting the rainfall event to allow for the 1 in 100 year plus 20% allowance for climate change indicate flooding from the system at MH AS12 close to plots 150-153. Flooding route would indicate that any flooding would flow westwards away from the dwelling and into the buffer zone area. Predicted flooding from the 1 in 100 year event plus 20% allowance for climate change is 36 m³ and would cover an area of approximately 3720 m² to a depth of 9.6mm. The predicted flooding depth from the 1 in 100 year plus 40% climate change would be 23mm. These areas would be within the soakage strata and therefore any flooding would be soak over time.

7 CLIMATE CHANGE

Surface water run-off has be calculated for the 1 in 100 year return period plus a 20% allowance for climate change. Any flooding for the 1 in 100 year return period with 40% allowance for climate change should be reviewed for potential flooding issues.

A 10% allowance for urban sprawl should also be factored into the calculations.

As the design and planning consent pre-dates the advice from Flood and Water Managements issued in June 2017, regarding using a modified FSR or FEH value has not been incorporated in the design, as discussed with FWM. However, estimates from the worst case system indicates that using the revised figures, these areas would be liable to flooding to a depth of 5.2mm across the surface area of the driveway, this depth of water would not be likely to run-off into the carriageways but be contained within the area covered by the permeable paving and eventually soak back into the permeable pavement.

8 POTENTIAL ADVERSE IMPACTS ON GROUNDWATER

Water Quality

The proposed land use for this site is residential thus there will be no pollution generated beyond the usual road runoff. This is likely to contain the following pollutants which would have varying effects on the receiving groundwater:-

- sediments
- metals (zinc, copper, cadmium)
- hydrocarbons (oil and fuel) including polycyclic aromatic hydrocarbons (PAH)
- pesticides and herbicides (from landscaping maintenance)
- chlorides (from de-icing).

The level of pollution associated with any runoff event depends on a number of factors including the type of site, the length of time since the last rainfall event (runoff that occurs after long dry periods will tend to be more polluted), and the duration and intensity of the rainfall itself.

Surface water runoff has higher concentrations of pollutants near the beginning of a storm, known as the "first flush", due to higher initial rainfall intensities, greater erosion potential and greater availability of solids and pollutants that have built up on urban surfaces during the preceding dry weather period. Consequently it is most important that the surface water from these storms is dealt with effectively.

9 MITIGATION STRATEGY

Water Quality

The SUDS Manual (CIRIA C697) recommends that the best solution for dealing with surface water runoff from a development is to mimic the natural catchment processes as closely as possible which is done by creating a "management train" of treatment processes. This concept is fundamental to designing a successful SUDS scheme — it uses drainage techniques in series to incrementally reduce pollution, flow rates and volumes.

Wherever possible, storm water should be managed as close to its source as possible rather than being conveyed to large systems at the bottom of drainage areas (end of pipe solutions). The techniques that are higher in the hierarchy are preferred to those further down so that prevention and control of water at source should always be considered before site or regional controls. However, where upstream control opportunities are restricted, a number of lower hierarchy options should be used in series. Water should be conveyed elsewhere only if it cannot be dealt with on site.

The SUDS Manual goes on to recommend the appropriate number of treatment processes for each area depending upon the end land use and the sensitivity of the receiving waters, ranging from low to high. Table 5.6, summarised below, indicates that for a receiving environment such as this the following numbers of treatment processes will be required

| | Table 5.6 |
|--------------------------------------|-----------|
| Receiving Water Sensitivity | MEDIUM |
| Runoff catchment | |
| Roofs Only | 1 |
| Residential Roads, Parking Areas, | 2 |

The current surface water drainage scheme for the development comprises two stages for the adoptable highways and residential parking and one stages for the roof area as listed below.

| Treatment Stage | Adoptable Roads | Residential Area Roads | Roofs |
|-----------------|-----------------|---------------------------|---------------------|
| 1 | Trapped Gully | Trapped Gully | Permeable Paving |
| 2 | Catchpits | Permeable Paving | |

The typical pollutants to be expected on this site as discussed earlier are likely to be

- sediments
- metals (zinc, copper, cadmium)
- hydrocarbons (oil and fuel) including polycyclic aromatic hydrocarbons (PAH)
- pesticides and herbicides (from landscaping maintenance)
- chlorides (from de-icing).

These need differing methods to remove them from the surface water.

Improvements to stormwater quality can be achieved by filtering the runoff using, for example, sand filters, gravels (e.g. permeable pavements, filter trenches), soils (e.g. bioretention), grasses and other surface vegetation (e.g. swales, detention basins) or aquatic vegetation (e.g. wetlands). The travel time or flow velocity through the system is specified to maximise treatment benefits.

Storing runoff volumes within detention basins contributes mainly to meeting the runoff rate criteria, but such systems also allow sedimentation to take place which contributes to water quality improvement.

Maintenance Requirements

It is essential that a regular maintenance programme is established and carried out to ensure the optimum performance of the SUDS elements. This will establish who owns each facility and who is responsible for its maintenance. It will also detail the required actions and the frequency with which they should be undertaken.

| Device | Location | Responsibility |
|---|---|---|
| Permeable Surfaces | Located within the curtilage of owner occupied properties | Freeholder of the property |
| Surfaces | Located within shared areas | Management company on behalf of the site owner. |
| Sediment sumps & Located within public highway vortex separator | | Kent Highways and or Southern water |
| Swales | Located within the Public open space | Management company on behalf of the site owner. |

Permeable Pavements

Permeable pavements provide hardstanding areas and roads suitable for vehicular traffic whilst allowing rainwater to infiltrate through the surface and into the underlying layers. The water is temporarily stored in a specially designed sub-base before discharge to a soakaway system. At this site they will be surfaced using concrete blocks designed for permeable systems.

Before handing over these pavements to the site owner they should be inspected for clogging, litter, weeds and water ponding and all failures should be rectified. After handover, the facility should be inspected regularly, preferably during and after heavy rainfall to check effective operation and to identify any areas of ponding.

Permeable surfaces need to be regularly cleaned of silt and other sediments so that their infiltration capacity is retained. CIRIA advise a minimum of three surface sweepings per year, as noted below, using a brush and suction cleaner, which can be a lorry-mounted device or a smaller precinct sweeper.

To prevent the loss of permeable areas form re-development or re-use, a covenant needs to be included in the sale to protect the integrity of the soakaways.

- 1. End of winter (April) to collect winter debris.
- 2. Mid-summer (July/August) to collect dust, flower and grass-type deposits.
- 3. After autumn leaf fall (November).

Care should be taken in adjusting vacuuming equipment to avoid removal of jointing material and any lost material should be replaced.

| Maintenance Schedule | Required action | Frequency |
|------------------------|---|--|
| Regular maintenance | Brushing and vacuuming. | Three times/year as described above, or as required based on site-specific observations of clogging or manufacturers' recommendations. |
| Occasional maintenance | Stabilise and mow contributing and adjacent areas. | As required |
| | Removal of weeds | As required |
| | Remediate any landscaping which, through vegetation maintenance or soil slip, has been raised to within 50 mm of the level of the paving. | As required |
| Remedial actions | Remedial work to any depressions or rutting and cracked or broken blocks considered detrimental to the structural performance or a hazard to users. | As required |
| | Rehabilitation of surface and upper sub-structure if infiltration performance is reduced as a result of significant clogging. | As required |
| Monitoring | Initial inspection Inspect for evidence of poor operation and/or weed growth. If required take remedial action. | Monthly for 3 months after installation 3-monthly and 48 h after large storms |
| | Inspect silt accumulation rates and establish appropriate brushing frequencies. | Annually. |

Catchpits and Hydrodynamic Vortex Separators

Catchpits should be inspected on an annual basis by lifting the cover of the inspection points to observe the condition of the base and the inlet points.

As with the soakaway chambers regular sweeping of all contributing hard surfaces will reduce the sediment load within the surface water discharge.

The table below summarises the recommended maintenance regime for catchpits on the site:-

| Maintenance Schedule | Required action | Frequency | |
|----------------------|--|---------------------------------|--|
| Regular maintenance | Debris removal from catchment surface (where may cause risks to performance) | Monthly | |
| | Remove sediment | Annually, or as required | |
| Remedial actions | Repair/rehabilitation of inlets, outlet, overflows and vents | As required | |
| Monitoring | Inspect/check all inlets, outlets, vents and overflows to ensure that they are in good condition and operating as designed | Annually and after large storms | |

10 FOUL WATER

The existing site has a number of connections onto the public foul sewer in Littlebourne Road. A capacity check with Southern Water has confirmed that there is not sufficient capacity within the existing public sewer for the whole of the new development and that upgrade works will be required or an alternate route provided for this site.

A section 98 application with Southern water undertaken and Southern Water have proposed a preferred connection onto the sewers in Chaucer Road which would not include offsite upgrade works. This would have sufficient capacity for the whole of the development. It is proposed to discharge 83 units located in phase 1 into Littlebourne Road, being the current compatible discharge volume and to take the remaining 418 units into Chaucer Road.

11 PHASES 2 AND 3

It is proposed to construct 500 dwellings with associated access roads and hardstanding areas in a three phase development. Phase 1 of the development has an impermeable are of approximately 58% of the total site area. Phase 2 and 3 have been apportioned appropriately.

The total impermeable area for the proposed development has been summarised in the table below.

| Impermeable Area | Total Area | Dwellings | Roofs | Private Drives | Shared Accesses | Public Highway |
|---------------------|---------------|-----------|--------|-------------------|--------------------|-------------------|
| PHASE 1 | 57,539 | 171 | 10,322 | 3,669 | 4,367 | 12,778 |
| PHASE 2# | 48,173 | 217 | 10,598 | 2,410 | 4,820 | 10,838 |
| PHASE 3# | 35,752 | 112 | 7,865 | 1,678 | 3,572 | 8,044 |
| SPINE ROAD | 7,414 | 0 | | | | |

based on projected areas from phase 1

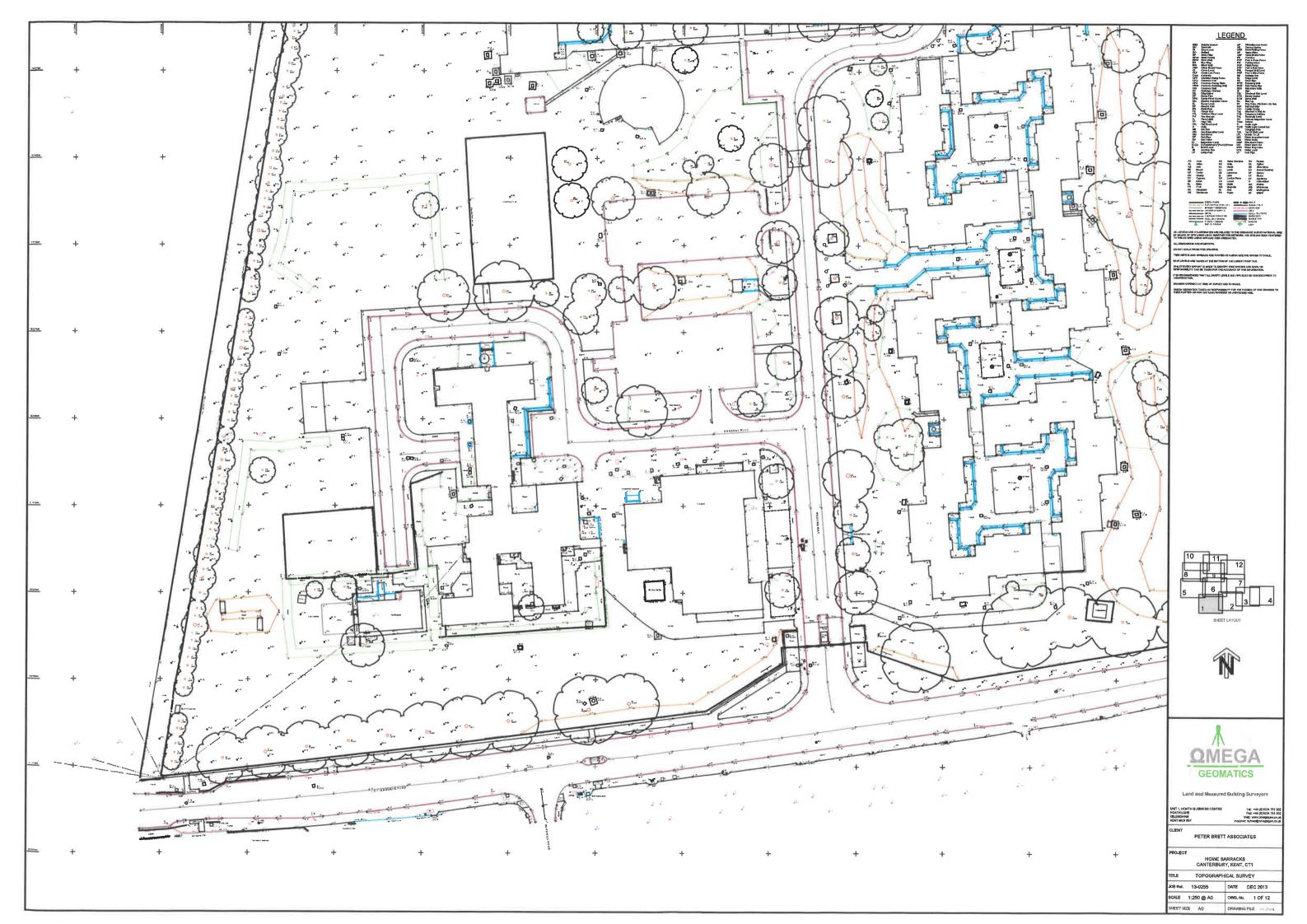
Phases 2 & 3 will be subject to a separate reserved matters application, each subject to its own detailed surface water drainage scheme. Current proposals anticipate using a similar strategy as used in the phase 1 development.

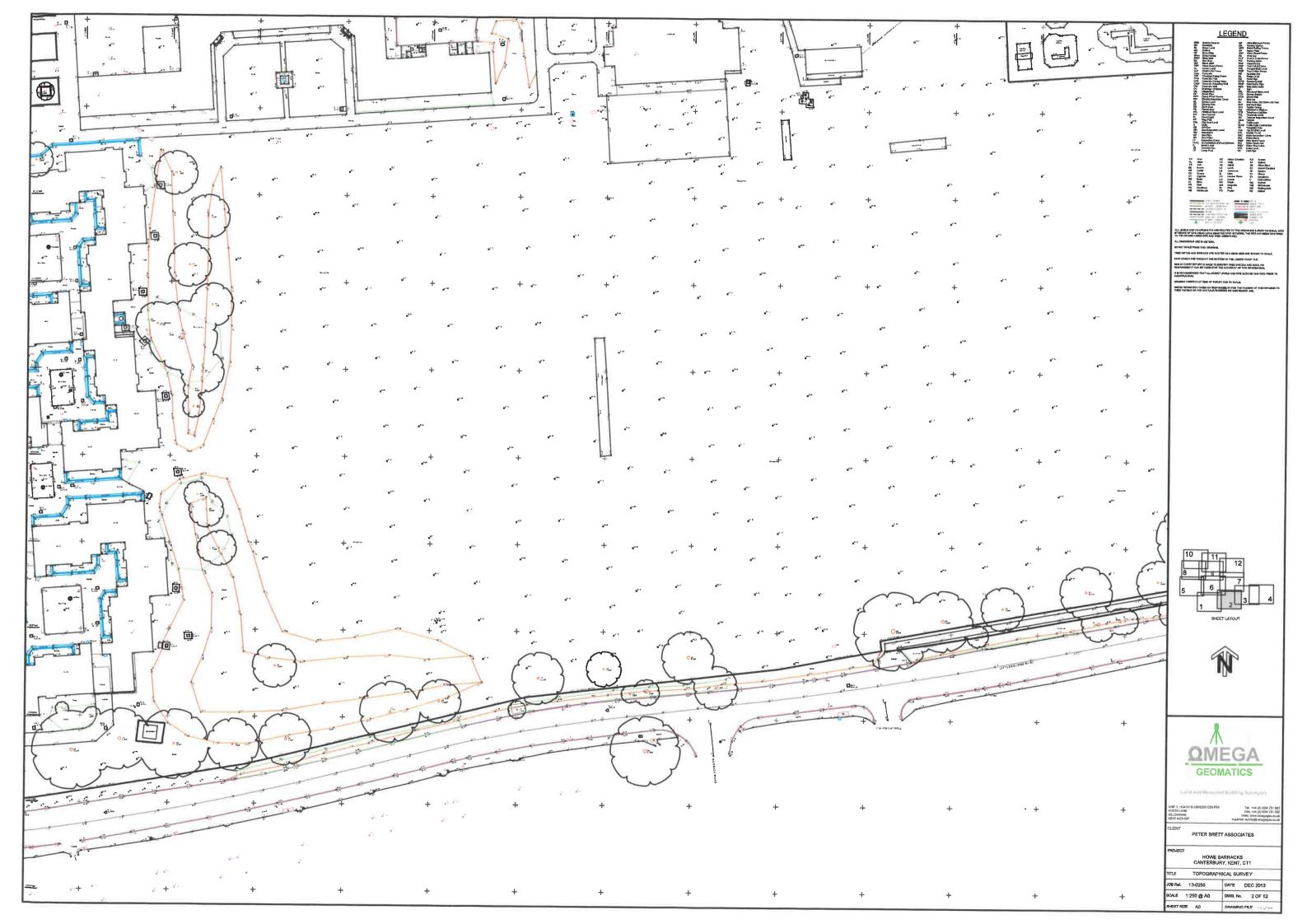
12 CONCLUSION

- The surface water from the site is currently being discharged into the public surface water sewer located in Littlebourne Road at an estimated peak rate of 115L/s and via deep soakaways located elsewhere on site.
- The deep soakaway are founded in the fine sands and although provide sufficient volumes for the current site would not meet the half drain time required for current standards.
- 3) Infiltration test carried out across the site suggest that infiltration within the shallow gravely clayey head deposits would provide sufficient infiltration for the residential units and private drives.
- 4) Surface water sewers are to be offered for adoption with Southern Water under a Section 104 agreement. Highway drainage is proposed to discharge into the onsite surface water sewers and into the existing surface water sewer in Littlebourne Road at a controlled rate of not more than 15L/s and 40l/s for the remaining phases. Attenuation and flow controls will limit peak surface water across the development to a maximum 55L/s based on Canterbury City Council's Brownfield run off rate. The existing highway drainage from Chaucer Road which is to be modified to account for the realignment of the carriageway is to be updated to accommodate the 1 in 100 year storm plus climate change.
- 5) In agreement with Southern Water, and as a site wide strategy it is proposed to discharge 418 units into the existing public foul water from the development into Chaucer Road and to discharge 83 units from Phase 1 into Littlebourne Road. Having undertaken a Section 98 agreement with Southern Water for these works it has been concluded that no upgrade works are required.

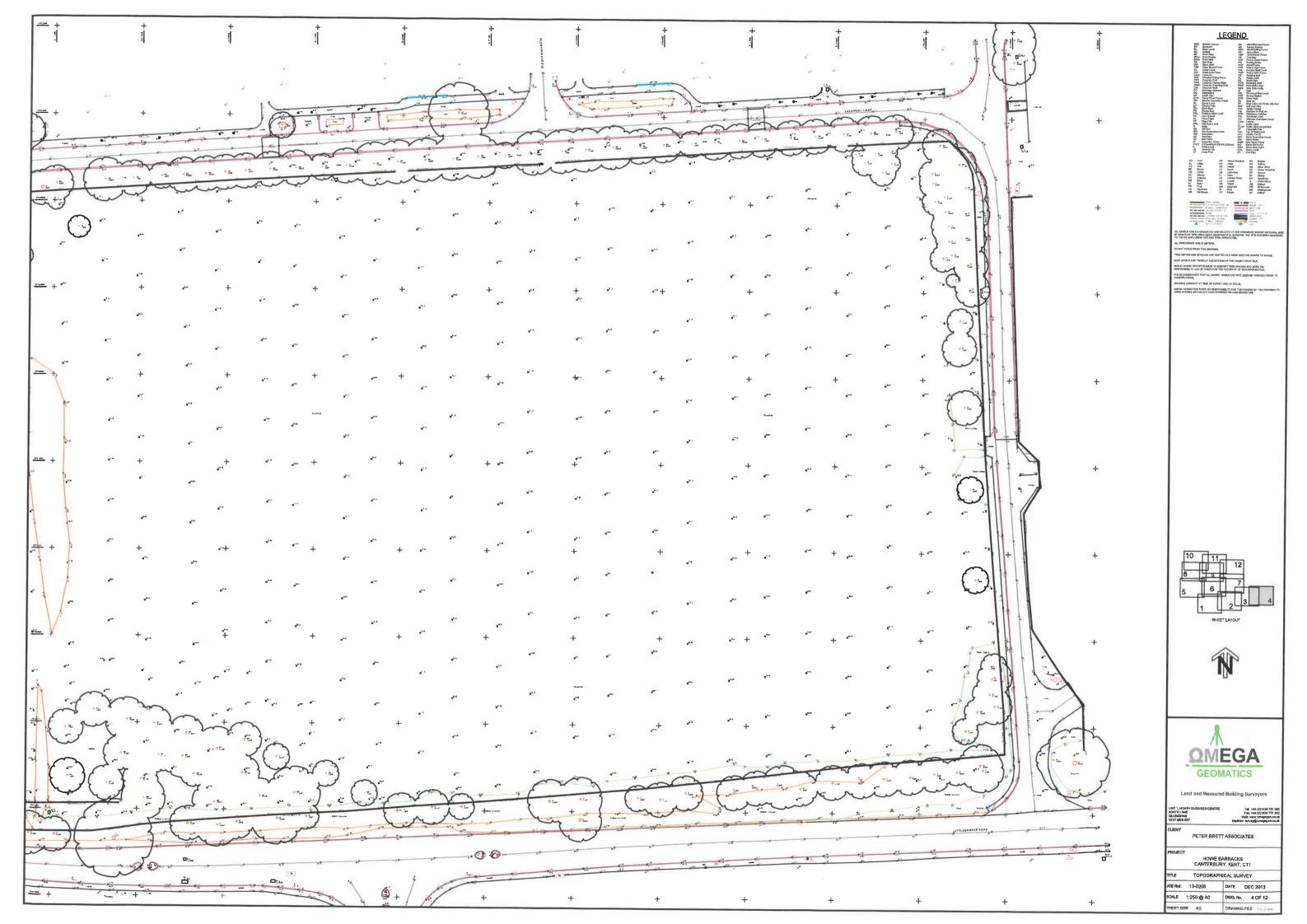
APPENDIX A

Existing Site Plan
Existing Utility Plan
Existing Contributing Areas
Borehole soakage rates
Greenfield Run-off Calculations
Sewer Records

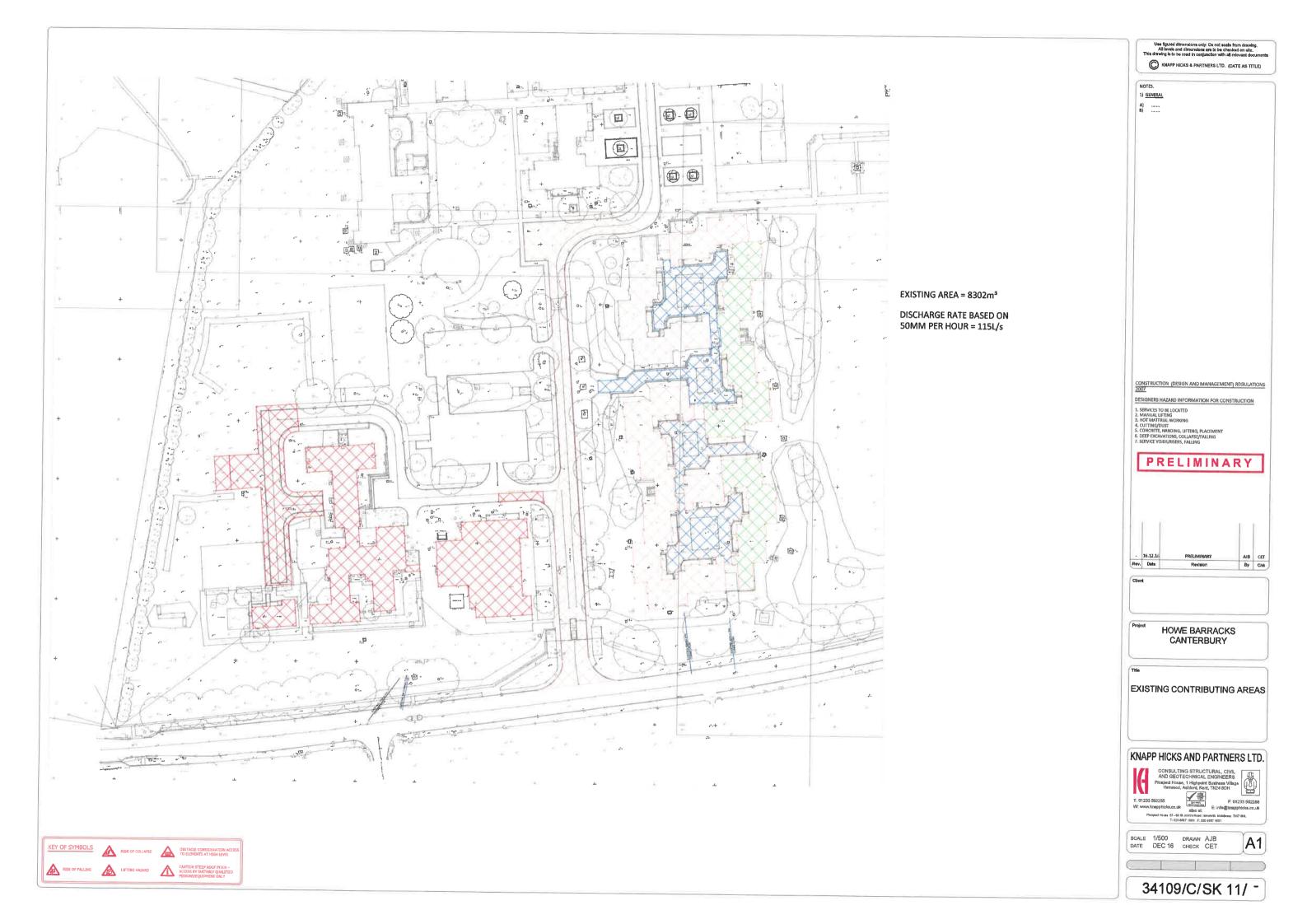


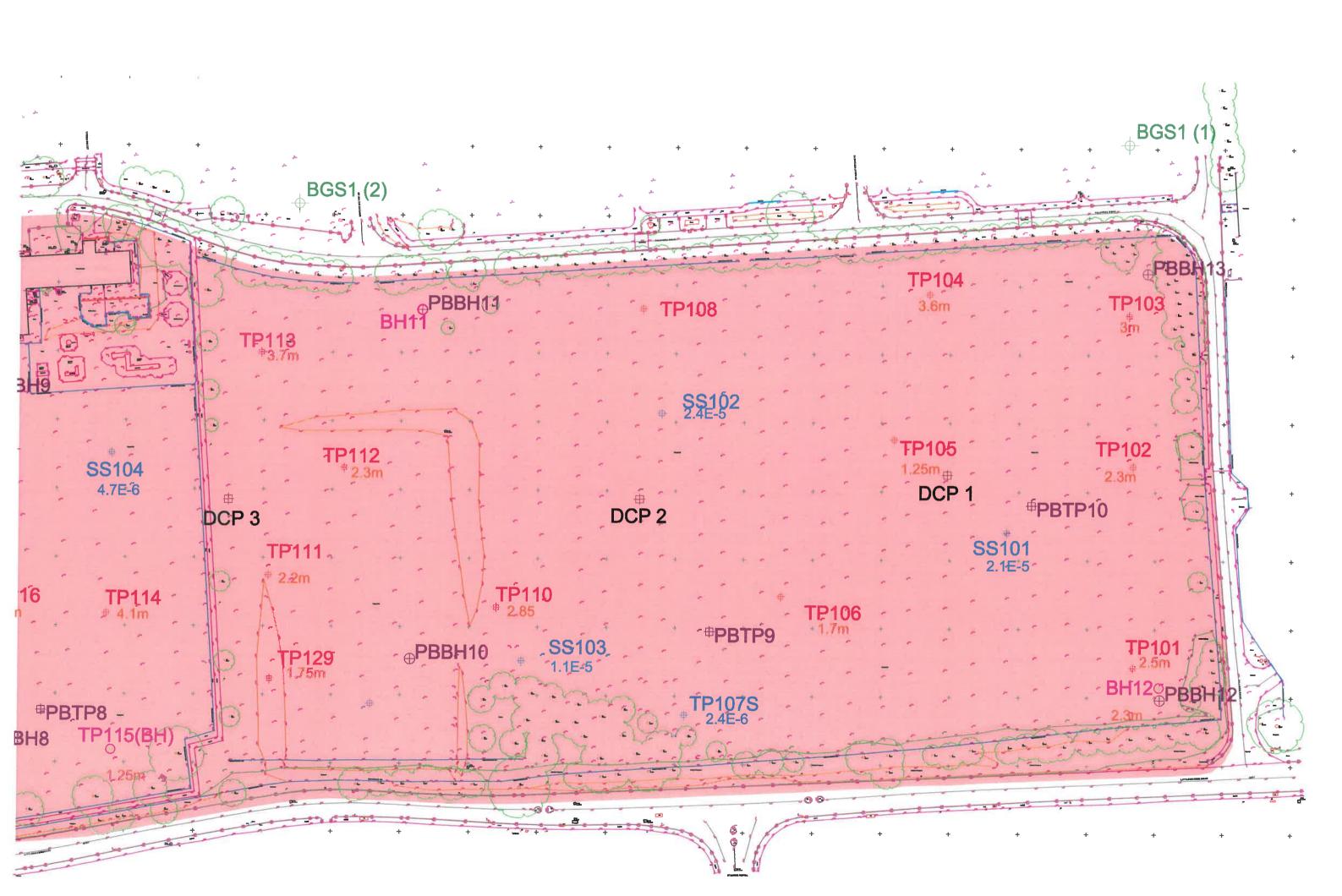












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| Kingston House | | rage 1 |
| Long Barrow Road | | |
| Orbital Park Ashford | | - |
| Date 07/12/2016 14:21 | Designed by andrewb | Micro |
| File | Checked by | Drainage |
| Causeway | Source Control 2015 1 | |

ICP SUDS Mean Annual Flood

Input

Return Period (years) 100 Soil 0.450 Area (ha) 19.000 Urban 0.000 SAAR (mm) 700 Region Number Region 7

Results 1/s

QBAR Rural 83.5 QBAR Urban 83.5

Q100 years 266.3

Q1 year 70.9 Q30 years 189.2 Q100 years 266.3

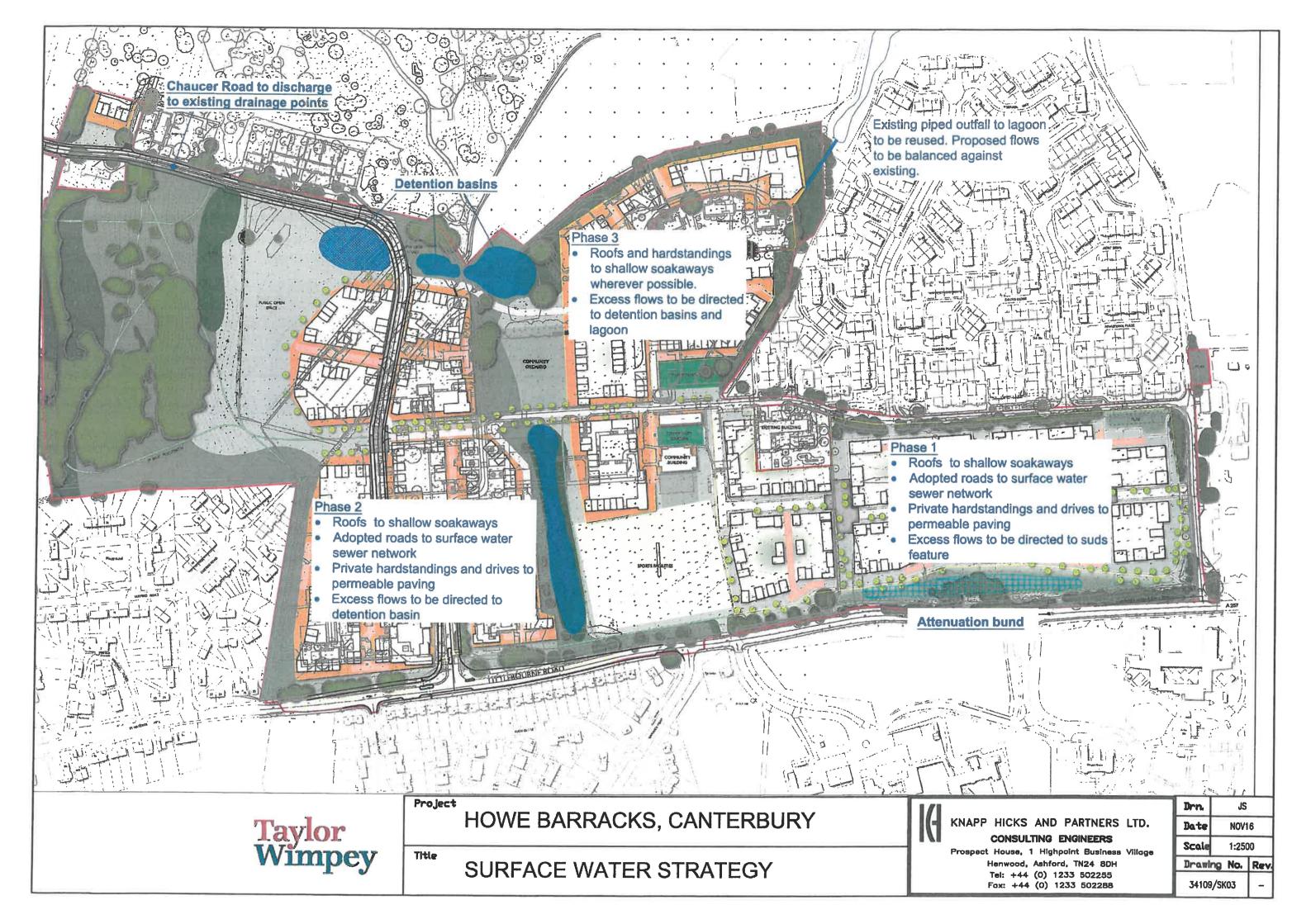


APPENDIX B

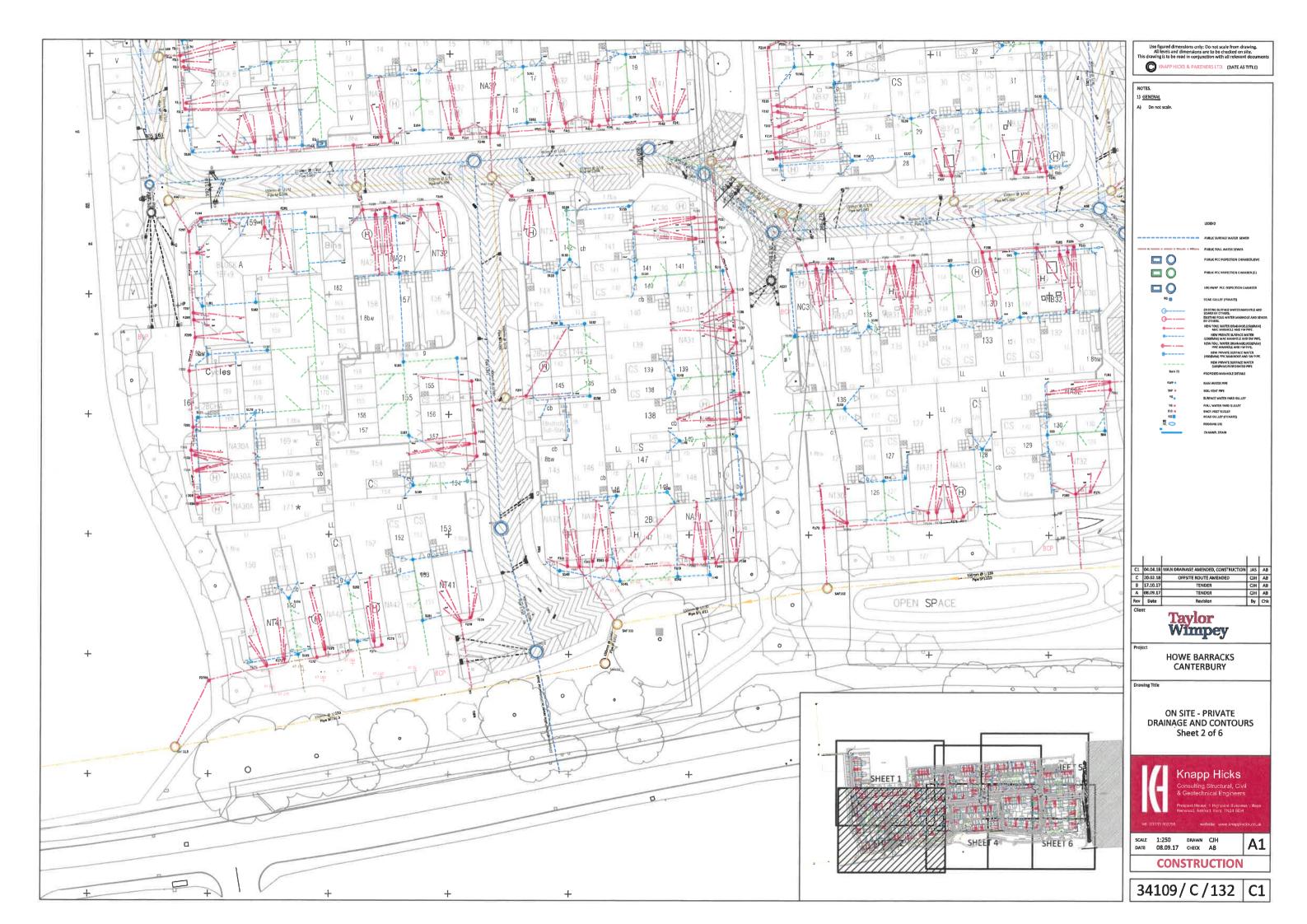
Proposed Master Plan
Permeable Area Plan
Phase1 Strategy
Overall Drainage Strategy
Proposed Foul Water Sewer
Surface water exceedance flows
Drainage schematic
Adoptable Highway Drainage Calculations

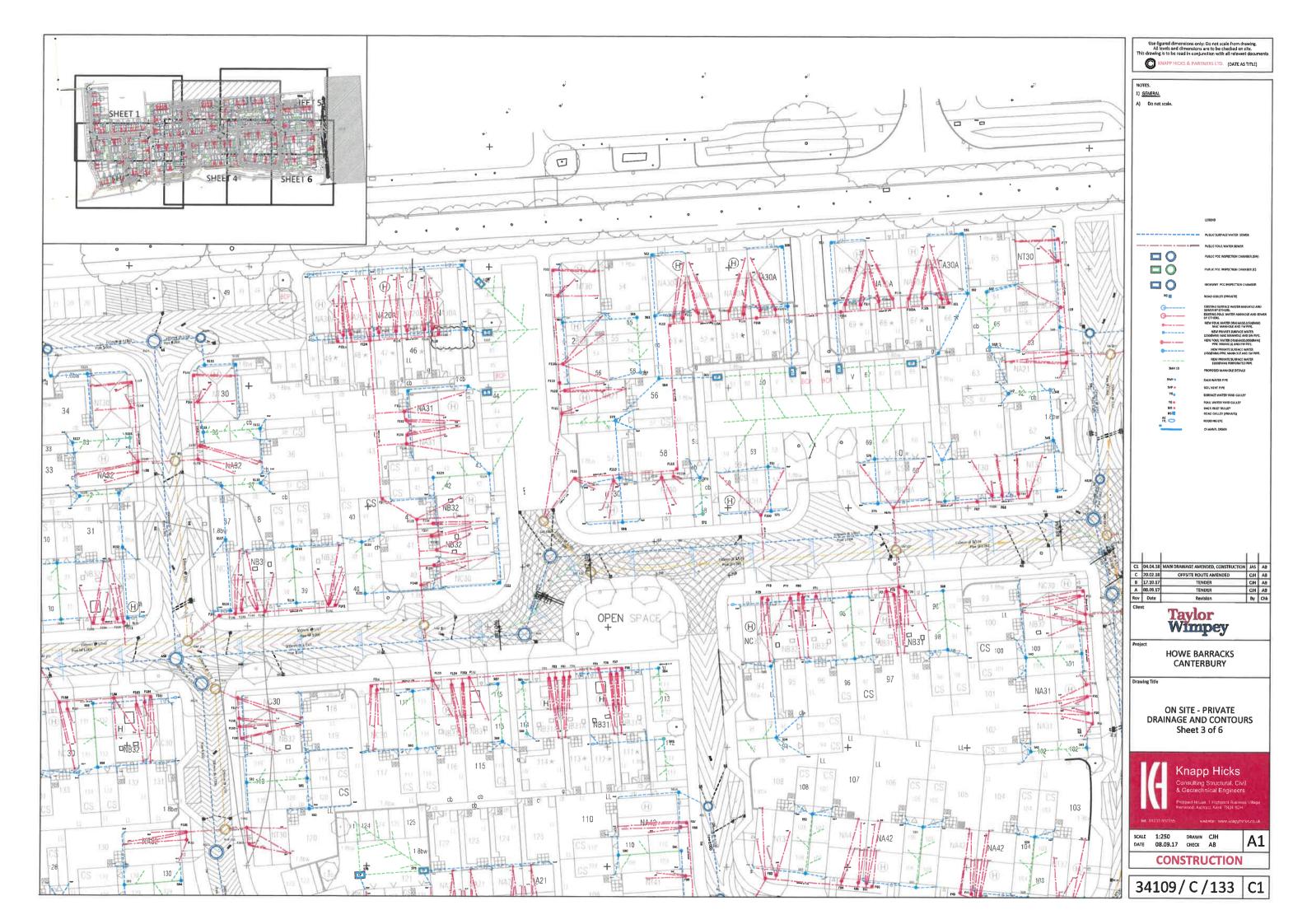






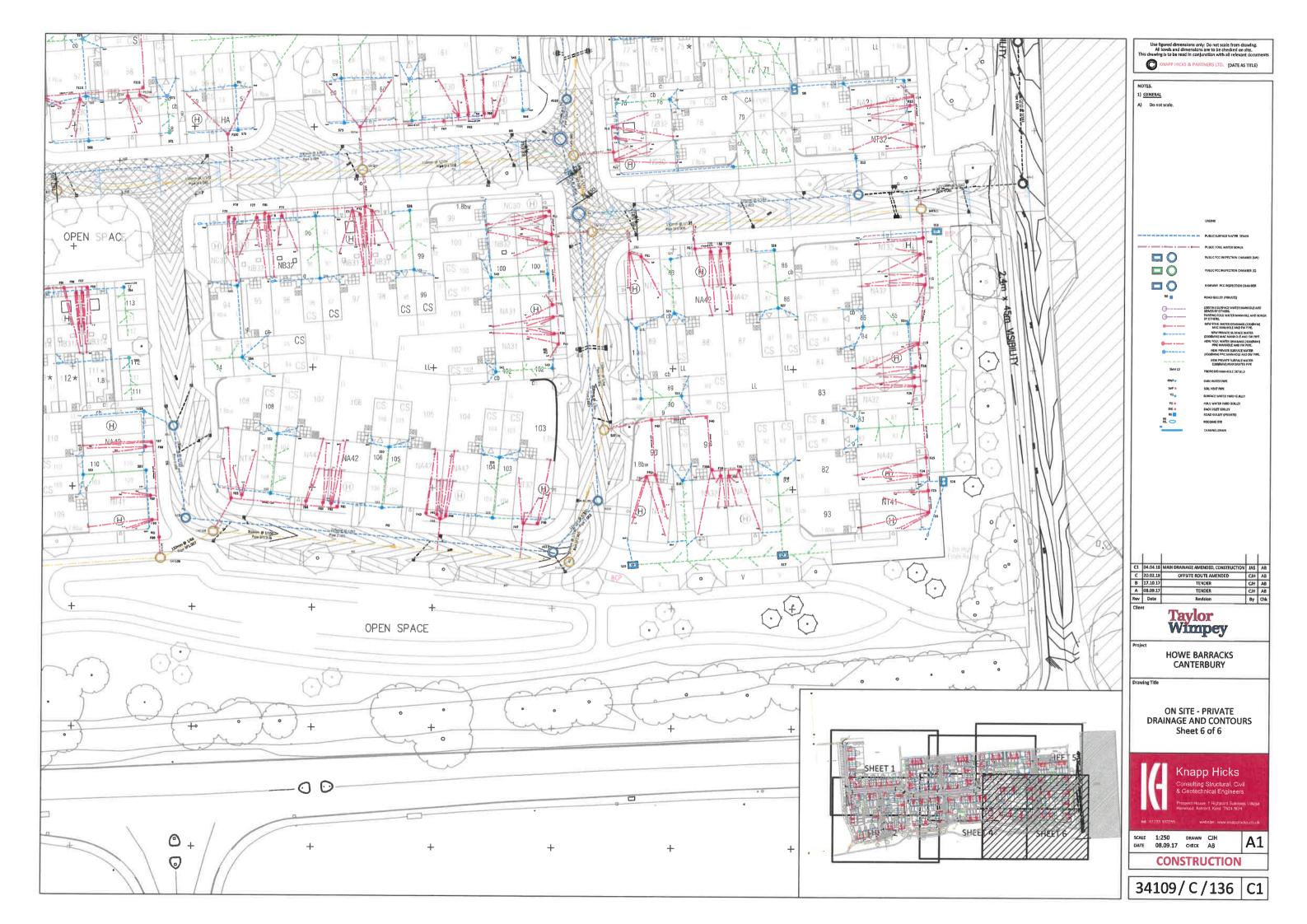


















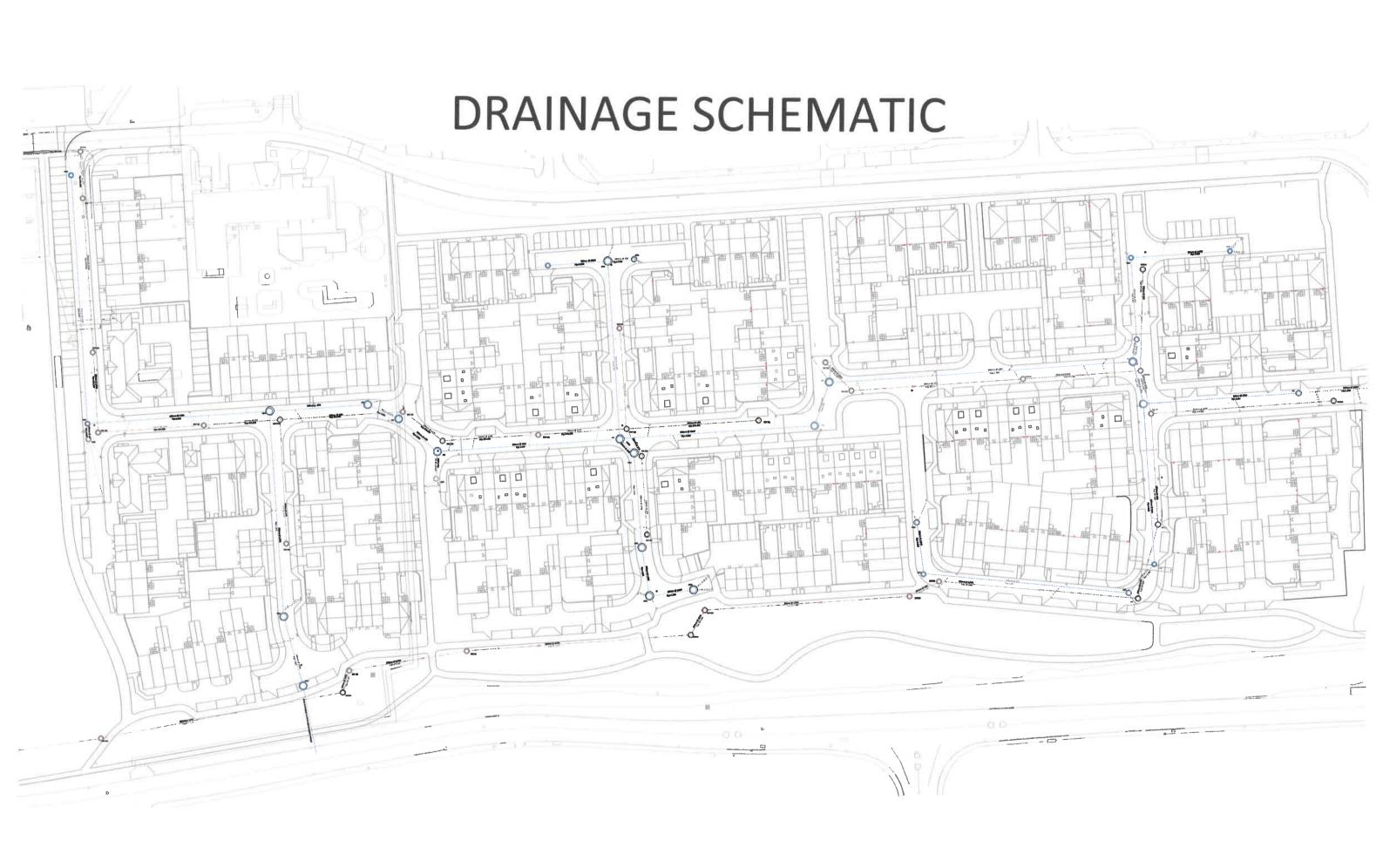








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| Long Barrow Road | | | | | |
| Orbital Park Ashford | | | | | Micro |
| Date 24/04/2018 15:29 | | Designed by andrewl | 0 | | Micro Drainage |
| File PHASE 1 SW REV.mdx Causeway | | Checked by | | | Didiridge |
| causeway | | Network 2015.1 | | | |
| | AS13 AS14 | | | AS28 | |
| | AS15 AS17 | | AS24 AS20 | E OND | |
| | AS16 1 1000 | | AS26S26 AS21 | AS2930 | |
| | AS18 | | AS22 | 8.00 t | |
| ASV2 MASV1 MAS AS1 | AS19 AS2 AS3 | AS4 AS5 | AS23 AS27 AS8 AS9 | AS10 IAIT | AS11 AS12 AS12A |
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| Kingston House | | |
| Long Barrow Road | | 4 |
| Orbital Park Ashford | | |
| Date 24/04/2018 14:34 | Designed by andrewb | Micto |
| File PHASE 1 SW REV.MDX | Checked by | Drainage |
| Causeway | Network 2015.1 | |

STORM SEWER DESIGN by the Modified Rational Method

Design Criteria for Storm

Pipe Sizes surfl Manhole Sizes STANDARD

FSR Rainfall Model - England and Wales

Return Period (years) 2 Add Flow / Climate Change (%) 0

M5-60 (mm) 19.800 Minimum Backdrop Height (m) 0.200

Ratio R 0.378 Maximum Backdrop Height (m) 1.500

Maximum Rainfall (mm/hr) 50 Min Design Depth for Optimisation (m) 1.200

Maximum Time of Concentration (mins) 30 Min Vel for Auto Design only (m/s) 1.000

Foul Sewage (1/s/ha) 0.000 Min Slope for Optimisation (1:X) 500

Volumetric Runoff Coeff. 0.750

Designed with Level Soffits

Time Area Diagram for Storm

| Time | Area | Time | Area | Time | Area |
|--------|-------|--------|-------|--------|-------|
| (mins) | (ha) | (mins) | (ha) | (mins) | (ha) |
| 0-4 | 0.374 | 4-8 | 0.627 | 8-12 | 0.064 |

Total Area Contributing (ha) = 1.066

Total Pipe Volume $(m^3) = 358.140$

Network Design Table for Storm

« - Indicates pipe capacity < flow

| PN | Length (m) | Fall (m) | Slope (1:X) | I.Area (ha) | | se (1/s) | k (mm) | HYD SECT | DIA (mm) | Auto Design |
|-------|---------------|-------------|-------------|----------------|------|-------------|-----------|-------------|-------------|----------------|
| | | | | | | | | | | _ |
| 1.000 | 23.607 | 0.145 | 162.8 | 0.021 | 5.00 | 0.0 | 0.600 | 0 | 225 | A |
| 1.001 | 27.460 | 0.170 | 161.5 | 0.046 | 0.00 | 0.0 | 0.600 | 0 | 225 | 8 |
| 1.002 | 46.782 | 0.285 | 164.1 | 0.033 | 0.00 | 0.0 | 0.600 | _ | 225 | ě |
| | | | | | | | | | | |
| | 15.503 | | 100.0 | 0.033 | 5.00 | 0.0 | 0.600 | 0 | 225 | |
| 2.001 | 61.381 | 0.630 | 97.4 | 0.054 | 0.00 | 0.0 | 0.600 | 0 | 225 | A |

Network Results Table

| PN | Rain (mm/hr) | T.C. (mins) | US/IL (m) | Σ I.Area (ha) | Σ Base Flow (1/s) | Foul (1/s) | Add Flow (1/s) | Vel (m/s) | Cap (1/s) | Flow (1/s) |
|-------|-----------------|----------------|--------------|------------------|----------------------|---------------|-------------------|--------------|--------------|---------------|
| 1.000 | 50.00 | 5.38 | 48.985 | 0.021 | 0.0 | 0.0 | 0.0 | 1.02 | 40.6 | 2.8 |
| 1.001 | 50.00 | 5.83 | 48.840 | 0.067 | 0.0 | 0.0 | 0.0 | 1.03 | 40.8 | 9.1 |
| 1.002 | 50.00 | 6.60 | 48.670 | 0.100 | 0.0 | 0.0 | 0.0 | 1.02 | | 13.5 |
| 2.000 | 50.00 | 5.20 | 50.035 | 0.033 | 0.0 | 0.0 | 0.0 | 1.31 | 52.0 | 4.5 |
| 2.001 | 50.00 | 5.97 | 49.880 | 0.087 | 0.0 | 0.0 | 0.0 | 1.32 | 52.7 | 11.8 |
| | | | ©1 | 982-201 | 5 XP Solu | ıtion | S | | | |

| Knapp Hicks & Partners Ltd | | Page 2 |
|----------------------------|---------------------|-------------|
| Kingston House | | |
| Long Barrow Road | | 4 |
| Orbital Park Ashford | | Villeton |
| Date 24/04/2018 14:34 | Designed by andrewb | Designation |
| File PHASE 1 SW REV.MDX | Checked by | Drainage |
| Causeway | Network 2015.1 | |

Network Design Table for Storm

| PN | Length | Fall | Slope | I.Area | T.E. | Base Flow (1/s) | k (mm) | HYD SECT | DIA (mm) | Auto Design |
|-------|--------|-------|-------|--------|------|--------------------|-----------|-------------|-------------|----------------|
| | | , , | | , , | | , , , , , , , | , | | ,, | |
| 2.002 | 11.439 | 0.115 | 99.5 | 0.016 | 0.00 | 0.0 | 0.600 | 0 | 225 | 6 |
| 2.003 | 47.915 | 0.750 | 63.9 | 0.069 | 0.00 | 0.0 | 0.600 | 0 | 300 | |
| 1.003 | 12.867 | 0.015 | 857.8 | 0.000 | 0.00 | 0.0 | 0.600 | 0 | 900 | 8 |
| 3.000 | 29.614 | A 195 | 151.9 | 0.045 | 5.00 | 0.0 | 0.600 | 0 | 225 | |
| 3.001 | 24.394 | 0.575 | 42.4 | 0.043 | 0.00 | | 0.600 | 0 | 225 | |
| 3.002 | 6.733 | | 44.9 | 0.000 | 0.00 | | 0.600 | 0 | 225 | |
| 3.002 | 0.755 | 0.150 | 11.7 | 0.000 | 0.00 | 0.0 | 0.000 | 0 | 225 | |
| 1.004 | 90.000 | 0.105 | 857.1 | 0.067 | 0.00 | 0.0 | 0.600 | 0 | 900 | 6 |
| 1.005 | 13.752 | 0.020 | 687.6 | 0.024 | 0.00 | 0.0 | 0.600 | 0 | 900 | 8 |
| 1.006 | 58.100 | 0.395 | 147.1 | 0.062 | 0.00 | 0.0 | 0.600 | 0 | 900 | 8 |
| | | | | | | | | | | |
| 4.000 | 13.301 | 0.015 | 886.7 | 0.022 | 5.00 | 0.0 | 0.600 | 0 | 900 | 8 |
| 4.001 | 14.639 | 0.025 | 585.6 | 0.027 | 0.00 | 0.0 | 0.600 | 0 | 900 | 6 |
| 4.002 | 28.242 | 0.040 | 706.1 | 0.043 | 0.00 | 0.0 | 0.600 | 0 | 900 | 6 |
| 4.003 | 5.941 | 0.195 | 30.5 | 0.000 | 0.00 | 0.0 | 0.600 | 0 | 900 | 6 |
| 5.000 | 17.797 | 0.110 | 161.8 | 0.032 | 5.00 | 0.0 | 0.600 | 0 | 225 | 8 |
| 6.000 | 7.769 | 0.445 | 17.5 | 0.018 | 5.00 | 0.0 | 0.600 | 0 | 225 | • |
| 5.001 | 53.115 | 1.490 | 35.6 | 0.046 | 0.00 | 0.0 | 0.600 | 0 | 900 | 6 |

Network Results Table

| PN | Rain (mm/hr) | T.C. | US/IL (m) | Σ | I.Area (ha) | ase (1/s) | Foul (1/s) | Add Flow (1/s) | Vel (m/s) | Cap | Flow (1/s) |
|-------|-----------------|------|--------------|---|----------------|--------------|---------------|----------------|--------------|--------|---------------|
| 2.002 | 50.00 | 6 12 | 49,250 | | 0.103 | 0.0 | 0.0 | 0.0 | 1.31 | 52.1 | 13.9 |
| 2.002 | 50.00 | | 49.060 | | 0.172 | 0.0 | 0.0 | 0.0 | 1.97 | 139.3 | 23.3 |
| 2.003 | 30.00 | 0.52 | 13.000 | | 0.172 | 0.0 | 0.0 | 0.0 | 1.57 | 139.3 | 23.3 |
| 1.003 | 50.00 | 6.80 | 47.710 | | 0.272 | 0.0 | 0.0 | 0.0 | 1.06 | 675.4 | 36.8 |
| | | | | | | | | | | | |
| 3.000 | 50.00 | 5.47 | 49.290 | | 0.045 | 0.0 | 0.0 | 0.0 | 1.06 | 42.1 | 6.1 |
| 3.001 | 50.00 | 5.67 | 49.095 | | 0.088 | 0.0 | 0.0 | 0.0 | 2.01 | 80.1 | 11.9 |
| 3.002 | 50.00 | 5.73 | 48.520 | | 0.088 | 0.0 | 0.0 | 0.0 | 1.96 | 77.8 | 11.9 |
| | | | | | | | | | | | |
| 1.004 | 50.00 | | 47.695 | | 0.427 | 0.0 | 0.0 | 0.0 | 1.06 | 675.7 | 57.8 |
| 1.005 | 50.00 | | 47.590 | | 0.451 | 0.0 | 0.0 | 0.0 | 1.19 | 755.3 | 61.1 |
| 1.006 | 50.00 | 8.78 | 47.570 | | 0.513 | 0.0 | 0.0 | 0.0 | 2.58 | 1642.3 | 69.5 |
| | | | 72.1 | | | | | | | | |
| 4.000 | 50.00 | | 47.450 | | 0.022 | 0.0 | 0.0 | 0.0 | 1.04 | 664.2 | 3.0 |
| 4.001 | 50.00 | | 47.435 | | 0.049 | 0.0 | 0.0 | 0.0 | 1.29 | 819.1 | 6.6 |
| 4.002 | 50.00 | | 47.410 | | 0.092 | 0.0 | 0.0 | 0.0 | 1.17 | 745.2 | 12.5 |
| 4.003 | 50.00 | 5.82 | 47.370 | | 0.092 | 0.0 | 0.0 | 0.0 | 5.69 | 3618.4 | 12.5 |
| | | | | | | | | | | | |
| 5.000 | 50.00 | 5.29 | 49.450 | | 0.032 | 0.0 | 0.0 | 0.0 | 1.03 | 40.8 | 4.3 |
| 6.000 | E0 00 | E 04 | 40 805 | | 0 010 | | | | | | <u>.</u> . |
| 6.000 | 50.00 | 5.04 | 49.785 | | 0.018 | 0.0 | 0.0 | 0.0 | 3.15 | 125.1 | 2.4 |
| 5.001 | 50.00 | 5 46 | 48.665 | | 0.096 | 0.0 | 0.0 | 0.0 | E 200 | 3344.5 | 12.0 |
| 3.001 | 50.00 | 5.40 | 20.000 | | 0.096 | 0.0 | 0.0 | 0.0 | 5.20 | 3344.5 | 13.0 |
| | | | 0. | | | | | | | | |

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| Knapp Hicks & Partners Ltd | | Page 3 |
|----------------------------|---------------------|-------------|
| Kingston House | | |
| Long Barrow Road | | 4 |
| Orbital Park Ashford | | Vilate |
| Date 24/04/2018 14:34 | Designed by andrewb | Designation |
| File PHASE 1 SW REV.MDX | Checked by | Drainage |
| Causeway | Network 2015 1 | 1 |

Network Design Table for Storm

| PN | Length | Fall | Slope | I.Area | T.E. | Base | k | HYD | DIA | Auto |
|-------|--------|-------|-------|--------|--------|------------|-------|------|------|--------|
| | (m) | (m) | (1:X) | (ha) | (mins) | Flow (1/s) | (mm) | SECT | (mm) | Design |
| | | | | | | | | | | |
| 1.007 | 54.412 | 1.215 | 44.8 | 0.061 | 0.00 | 0.0 | 0.600 | 0 | 900 | 8 |
| | | | | | | | | | | |
| 7.000 | 8.020 | 1.325 | 6.1 | 0.015 | 5.00 | 0.0 | 0.600 | 0 | 225 | |
| | | | | | | | | | | |
| 1.008 | 15.103 | 0.335 | 45.1 | 0.000 | 0.00 | 0.0 | 0.600 | 0 | 900 | 8 |
| 1.009 | 10.146 | 0.240 | 42.3 | 0.026 | 0.00 | 0.0 | 0.600 | 0 | 900 | |
| 1.010 | 29.122 | 0.545 | 53.4 | 0.019 | 0.00 | 0.0 | 0.600 | 0 | 900 | |
| | | | | | | | | | | |
| 8.000 | 74.053 | 0.435 | 170.2 | 0.072 | 5.00 | 0.0 | 0.600 | 0 | 600 | |
| | | | | | | | | | | |
| 9.000 | 4.645 | 0.895 | 5.2 | 0.021 | 5.00 | 0.0 | 0.600 | 0 | 225 | 8 |
| P 001 | 54.212 | 0 200 | 140 7 | 0.059 | 0.00 | 0.0 | 0.600 | _ | | |
| 6.001 | 34.212 | 0.360 | 142./ | 0.059 | 0.00 | 0.0 | 0.600 | 0 | 600 | 6 |
| 1.011 | 61.354 | 0.205 | 299.3 | 0.036 | 0.00 | 0.0 | 0.600 | 0 | 900 | |
| 1.012 | 21.422 | 0.075 | 285.6 | 0.021 | 0.00 | 0.0 | 0.600 | 0 | 900 | ě |
| 1.013 | 20.673 | 0.130 | 159.0 | 0.035 | 0.00 | | 0.600 | 0 | 225 | ě |
| | | | | | | | | - | | |

Network Results Table

| PN | Rain | T.C. | US/IL | Σ I.Area | Σ Base | Foul | Add Flow | Vel | Cap | Flow |
|-------|---------|--------|--------|----------|------------|-------|----------|-------|--------|-------|
| | (mm/hr) | (mins) | (m) | (ha) | Flow (1/s) | (l/s) | (1/s) | (m/s) | (1/s) | (1/s) |
| | | | | | | | | | | |
| 1.007 | 50.00 | 8.97 | 47.175 | 0.762 | 0.0 | 0.0 | 0.0 | 4.69 | 2983.0 | 103.2 |
| 7.000 | 50.00 | 5.02 | 47.960 | 0.015 | 0.0 | 0.0 | 0.0 | 5.35 | 212.9 | 2.0 |
| 1.008 | 50.00 | 9.03 | 45.960 | 0.777 | 0.0 | 0.0 | 0.0 | 4.67 | 2973.1 | 105.2 |
| 1.009 | 50.00 | 9.06 | 45.625 | 0.803 | 0.0 | 0.0 | 0.0 | 4.83 | 3070.5 | |
| 1.010 | 50.00 | 9.18 | 45.385 | 0.822 | 0.0 | 0.0 | 0.0 | 4.29 | 2730.2 | 111.3 |
| | | | | | | | | | | |
| 8.000 | 50.00 | 5.66 | 45.955 | 0.072 | 0.0 | 0.0 | 0.0 | 1.86 | 526.9 | 9.7 |
| 9.000 | 50.00 | F 01 | 46.790 | 0.001 | | | | | | |
| 9.000 | 50.00 | 5.01 | 46.790 | 0.021 | 0.0 | 0.0 | 0.0 | 5.78 | 229.9 | 2.8 |
| 8.001 | 50.00 | 6.11 | 45.520 | 0.152 | 0.0 | 0.0 | 0.0 | 2.04 | 575.9 | 20.6 |
| | | | | | | | *** | | 0.013 | |
| 1.011 | 49.29 | 9.74 | 44.840 | 1.010 | 0.0 | 0.0 | 0.0 | 1.81 | 1148.9 | 134.8 |
| 1.012 | 48.79 | 9.93 | 44.635 | 1.031 | 0.0 | 0.0 | 0.0 | 1.85 | 1176.2 | 136.2 |
| 1.013 | 47.96 | 10.27 | 44.560 | 1.066 | 0.0 | 0.0 | 0.0 | 1.03 | 41.1« | 138.5 |

| Knapp Hicks & Partners Ltd | | Page 4 |
|----------------------------|---------------------|----------|
| Kingston House | | |
| Long Barrow Road | | 4 |
| Orbital Park Ashford | | Missis |
| Date 24/04/2018 14:34 | Designed by andrewb | Desipage |
| File PHASE 1 SW REV.MDX | Checked by | Drainage |
| Causeway | Network 2015.1 | |

Manhole Schedules for Storm

| MH Name | MH CL (m) | MH Depth (m) | MH Connection | MH Diam.,L*W (mm) | PN | Pipe Out Invert Level (m) | Diameter (mm) | PN | Pipes In Invert Level (m) | Diameter (mm) | Ва | ckdro |
|------------|--------------|--------------------|------------------|-------------------------|-------|---------------------------------|---------------|-------|---------------------------------|---------------|----|-------|
| ASV2 | 50.590 | 1.605 | Open Manhole | 1200 | 1.000 | 48.985 | 225 | | | | | |
| ASV1 | 50.530 | 1.690 | Open Manhole | 1200 | 1.001 | 48.840 | 225 | 1.000 | 48.840 | 225 | | |
| AS1 | 50.302 | 1.632 | Open Manhole | 1200 | 1.002 | 48.670 | 225 | 1.001 | 48.670 | 225 | | |
| AS13 | 51.424 | 1.389 | Open Manhole | 1200 | 2.000 | 50.035 | 225 | | | | | |
| AS14 | 51.299 | 1.419 | Open Manhole | 1200 | 2.001 | 49.880 | 225 | 2.000 | 49.880 | 225 | | |
| AS15 | 50.846 | 1.596 | Open Manhole | 1200 | 2.002 | 49.250 | 225 | 2.001 | 49.250 | 225 | | |
| AS16 | 50.744 | 1.684 | Open Manhole | 1200 | 2.003 | 49.060 | 300 | 2.002 | 49.135 | 225 | | |
| AS2 | 50.829 | 3.119 | Open Manhole | 1800 | 1.003 | 47.710 | 900 | 1.002 | 48.385 | 225 | | |
| | | | | | | | | 2.003 | 48.310 | 300 | | |
| AS17 | 50.717 | 1.427 | Open Manhole | 1200 | 3.000 | 49.290 | 225 | | | | | |
| AS18 | 50.964 | 1.869 | Open Manhole | 1200 | 3.001 | 49.095 | 225 | 3.000 | 49.095 | 225 | | |
| AS19 | 50.842 | 2.322 | Open Manhole | 1200 | 3.002 | 48.520 | 225 | 3.001 | 48.520 | 225 | | |
| AS3 | 50.989 | 3.294 | Open Manhole | 1800 | 1.004 | 47.695 | 900 | 1.003 | 47.695 | 900 | | |
| | | | | | | | | 3.002 | 48.370 | 225 | | |
| AS4 | 51.728 | 4.138 | Open Manhole | 1800 | 1.005 | 47.590 | 900 | 1.004 | 47.590 | 900 | | |
| AS5 | 51.624 | 4.054 | Open Manhole | 1800 | 1.006 | 47.570 | 900 | 1.005 | 47.570 | 900 | | |
| AS20 | 49.578 | 2.128 | Open Manhole | 1800 | 4.000 | 47.450 | 900 | | | | | |
| AS21 | 49.646 | 2.211 | Open Manhole | 1800 | 4.001 | 47.435 | 900 | 4.000 | 47.435 | 900 | | |
| AS22 | 50.014 | 2.604 | Open Manhole | 1800 | 4.002 | 47.410 | 900 | 4.001 | 47.410 | 900 | | |
| AS23 | 50.832 | 3.462 | Open Manhole | 1800 | 4.003 | 47.370 | 900 | 4.002 | 47.370 | 900 | | |
| AS24 | 51.175 | 1.725 | Open Manhole | 1200 | 5.000 | 49.450 | 225 | | | | | |
| AS26 | 51.510 | 1.725 | Open Manhole | 1200 | 6.000 | 49.785 | 225 | | | | | |
| AS25 | 51.409 | 2.744 | Open Manhole | 1800 | 5.001 | 48.665 | 900 | 5.000 | 49.340 | 225 | | |
| | | | | | | | | 6.000 | 49.340 | 225 | П | |
| AS6 | 50.926 | 3.751 | Open Manhole | 1800 | 1.007 | 47.175 | 900 | 1.006 | 47.175 | 900 | | |
| | | | | | | | | 4.003 | 47.175 | 900 | | |
| | | | | | | | | 5.001 | 47.175 | 900 | | |
| AS27 | 49.664 | 1.704 | Open Manhole | 1200 | 7.000 | 47.960 | 225 | | | | | |
| AS7 | 49.939 | 3.979 | Open Manhole | 1800 | 1.008 | 45.960 | 900 | 1.007 | 45.960 | 900 | | |
| | | | | | | | | 7.000 | 46.635 | 225 | | |
| AS8 | 49.624 | 3.999 | Open Manhole | 1800 | 1.009 | 45.625 | 900 | 1.008 | 45.625 | 900 | | |
| AS9 | 49.360 | 3.975 | Open Manhole | 1800 | 1.010 | 45.385 | 900 | 1.009 | 45.385 | 900 | | |
| AS28 | 47.862 | 1.907 | Open Manhole | 1500 | 8.000 | 45.955 | 600 | | | | | |
| AS30 | 47.767 | 0.977 | Open Manhole | 1200 | 9.000 | 46.790 | 225 | | | | | |
| AS29 | 47.750 | 2.230 | Open Manhole | 1500 | 8.001 | 45.520 | 600 | 8.000 | 45.520 | 600 | | |
| | | | | | | | | 9.000 | 45.895 | 225 | | |
| AS10 | 48.615 | 3.775 | Open Manhole | 1800 | 1.011 | 44.840 | 900 | 1.010 | 44.840 | 900 | | |
| | 1 | | | | | | | 8.001 | 45.140 | 600 | | |
| AS11 | 47.750 | 3.115 | Open Manhole | 1800 | 1.012 | 44.635 | 900 | 1.011 | 44.635 | 900 | | |
| | A | 72 U | | ©1982-2 | 015 X | P Soluti | ons. | | | 10 | - | |

| Knapp Hicks & Partners Ltd | | Page 5 |
|----------------------------|---------------------|-------------|
| Kingston House | | |
| Long Barrow Road | | 4 |
| Orbital Park Ashford | | Villega |
| Date 24/04/2018 14:34 | Designed by andrewb | Designation |
| File PHASE 1 SW REV.MDX | Checked by | Drainage |
| Causeway | Network 2015.1 | |

Manhole Schedules for Storm

| MH Name | MH CL (m) | MH Depth (m) | MH Connection | MH Diam.,L*W (mm) | PN | Pipe Out Invert Level (m) | Diameter (mm) | PN | Pipes In Invert Level (m) | Diameter (mm) | Backdrop (mm) |
|------------|------------------|--------------------|------------------------------|-------------------------|-------|---------------------------------|------------------|----------------|---------------------------------|------------------|------------------|
| | 47.862 46.100 | | Open Manhole Open Manhole | | 1.013 | 44.560 OUTFALL | 225 | 1.012 1.013 | 44.560 44.430 | 900 225 | |

Simulation Criteria for Storm

Volumetric Runoff Coeff 0.750 Additional Flow - % of Total Flow 0.000
Areal Reduction Factor 1.000 MADD Factor * 10m³/ha Storage 2.000
Hot Start (mins) 0 Inlet Coefficient 0.800
Hot Start Level (mm) 0 Flow per Person per Day (1/per/day) 0.000
Manhole Headloss Coeff (Global) 0.500 Run Time (mins) 60
Foul Sewage per hectare (1/s) 0.000 Output Interval (mins) 1

Number of Input Hydrographs 0 Number of Offline Controls 0 Number of Time/Area Diagrams 0 Number of Online Controls 8 Number of Storage Structures 0 Number of Real Time Controls 0

Synthetic Rainfall Details

| Rainfall Model | FSR | Profile Type | Summer |
|-----------------------|-------------------|-----------------------|--------|
| Return Period (years) | 2 | Cv (Summer) | 0.750 |
| Region | England and Wales | Cv (Winter) | 0.840 |
| M5-60 (mm) | 19.800 | Storm Duration (mins) | 30 |
| Ratio R | 0.378 | | |

| Knapp Hicks & Partners Ltd | | Page 6 |
|----------------------------|---------------------|----------|
| Kingston House | | |
| Long Barrow Road | | 4 |
| Orbital Park Ashford | | Mileson |
| Date 24/04/2018 14:34 | Designed by andrewb | Drainage |
| File PHASE 1 SW REV.MDX | Checked by | Drainage |
| Causeway | Network 2015.1 | 1/1 |

Online Controls for Storm

Orifice Manhole: AS5, DS/PN: 1.006, Volume (m³): 17.9

Diameter (m) 0.115 Discharge Coefficient 0.600 Invert Level (m) 47.570

Orifice Manhole: AS22, DS/PN: 4.002, Volume (m³): 14.8

Diameter (m) 0.115 Discharge Coefficient 0.600 Invert Level (m) 47.410

Orifice Manhole: AS23, DS/PN: 4.003, Volume (m³): 25.6

Diameter (m) 0.115 Discharge Coefficient 0.600 Invert Level (m) 47.370

Orifice Manhole: AS6, DS/PN: 1.007, Volume (m³): 80.6

Diameter (m) 0.115 Discharge Coefficient 0.600 Invert Level (m) 47.175

Orifice Manhole: AS7, DS/PN: 1.008, Volume (m³): 43.9

Diameter (m) 0.115 Discharge Coefficient 0.600 Invert Level (m) 45.960

Orifice Manhole: AS8, DS/PN: 1.009, Volume (m³): 18.6

Diameter (m) 0.115 Discharge Coefficient 0.600 Invert Level (m) 45.625

Orifice Manhole: AS9, DS/PN: 1.010, Volume (m³): 15.4

Diameter (m) 0.115 Discharge Coefficient 0.600 Invert Level (m) 45.385

Hydro-Brake® Manhole: AS12, DS/PN: 1.013, Volume (m³): 20.9

Design Head (m) 2.760 Hydro-Brake® Type Md6 SW Only Invert Level (m) 44.560 Design Flow (l/s) 14.0 Diameter (mm) 121

| Depth (m) F | Plow (1/s) | Depth (m) | Flow (1/s) | Depth (m) | Flow (1/s) | Depth (m) | Flow (1/s) |
|-------------|------------|-----------|------------|-----------|------------|-----------|------------|
| | | | | | | | |
| 0.100 | 3.9 | 1.200 | 9.2 | 3.000 | 14.5 | 7.000 | 22.1 |
| 0.200 | 7.4 | 1.400 | 9.9 | 3.500 | 15.6 | 7.500 | 22.9 |
| 0.300 | 7.6 | 1.600 | 10.6 | 4.000 | 16.7 | 8.000 | 23.6 |
| 0.400 | 7.3 | 1.800 | 11.2 | 4.500 | 17.7 | 8.500 | 24.4 |
| 0.500 | 7.1 | 2.000 | 11.8 | 5.000 | 18.7 | 9.000 | 25.1 |
| 0.600 | 7.1 | 2.200 | 12.4 | 5.500 | 19.6 | 9.500 | 25.7 |
| 0.800 | 7.7 | 2.400 | 12.9 | 6.000 | 20.5 | | |
| 1.000 | 8.4 | 2.600 | 13.5 | 6.500 | 21.3 | | |

| Knapp Hicks & Partners Ltd | | Page 7 | | |
|----------------------------|---------------------|-----------|--|--|
| Kingston House | | | | |
| Long Barrow Road | | ~ | | |
| Orbital Park Ashford | | Mirro | | |
| Date 24/04/2018 14:34 | Designed by andrewb | Drainage | | |
| File PHASE 1 SW REV.MDX | Checked by | Didirioge | | |
| Causeway | Network 2015.1 | | | |

Summary of Critical Results by Maximum Level (Rank 1) for Storm

Simulation Criteria

Areal Reduction Factor 1.000 Additional Flow - % of Total Flow 0.000

Hot Start (mins) 0 MADD Factor * 10m³/ha Storage 2.000

Hot Start Level (mm) 0 Inlet Coefficient 0.800

Manhole Headloss Coeff (Global) 0.500 Flow per Person per Day (1/per/day) 0.000

Foul Sewage per hectare (1/s) 0.000

Number of Input Hydrographs 0 Number of Offline Controls 0 Number of Time/Area Diagrams 0 Number of Online Controls 8 Number of Storage Structures 0 Number of Real Time Controls 0

Synthetic Rainfall Details

Rainfall Model FSR Ratio R 0.379
Region England and Wales Cv (Summer) 0.750
M5-60 (mm) 19.800 Cv (Winter) 0.840

Margin for Flood Risk Warning (mm) 300.0

Analysis Timestep 2.5 Second Increment (Extended)

DTS Status

DVD Status

ON

Inertia Status

Profile(s) Summer and Winter
Duration(s) (mins) 15, 30, 60, 120, 180, 240, 360, 480, 600, 720, 960, 1440, 2160, 2880, 4320, 5760, 7200, 8640, 10080

Return Period(s) (years) 30
Climate Change (%) Summer and Winter
Summer and Winter
15, 30, 60, 120, 180, 240, 360, 480, 600, 720, 960, 1440, 2160, 2880, 4320, 5760, 7200, 8640, 10080
30

| PN | US/MH Name | s | torm | | Climate Change | First Surch | | First (Y) Flood | First (Z) Overflow | Overflow Act. | Water Level (m) |
|-------|---------------|-----|--------|----|-------------------|----------------|--------|--------------------|-----------------------|------------------|-----------------------|
| 1.000 | ASV2 | 60 | Winter | 30 | +30% | 30/30 | Winter | | | | 49.468 |
| 1.001 | ASV1 | 60 | Winter | 30 | +30% | 30/30 | Winter | | | | 49.465 |
| 1.002 | AS1 | 60 | Winter | 30 | +30% | 30/15 | Summer | | | | 49.456 |
| 2.000 | AS13 | 15 | Winter | 30 | +30% | | | | | | 50.121 |
| 2.001 | AS14 | 15 | Winter | 30 | +30% | | | | | | 50.029 |
| 2.002 | AS15 | 60 | Winter | 30 | +30% | | | | | | 49.463 |
| 2.003 | AS16 | 60 | Winter | 30 | +30% | 30/60 | Winter | | | | 49.454 |
| 1.003 | AS2 | 60 | Winter | 30 | +30% | 30/15 | Winter | | | | 49.438 |
| 3.000 | AS17 | 60 | Winter | 30 | +30% | | | | | | 49.461 |
| 3.001 | AS18 | 60 | Winter | 30 | +30% | 30/60 | Winter | | | | 49.454 |
| 3.002 | AS19 | 60 | Winter | 30 | +30% | 30/30 | Summer | | | | 49.442 |
| 1.004 | AS3 | 60 | Winter | 30 | +30% | 30/15 | Winter | | | | 49.437 |
| 1.005 | AS4 | 60 | Winter | 30 | +30% | 30/15 | Winter | | | | 49.434 |
| 1.006 | AS5 | 60 | Winter | 30 | +30% | 30/15 | Winter | | | | 49.432 |
| 4.000 | AS20 | 240 | Winter | 30 | +30% | 30/240 | Winter | | | | 48.358 |
| 4.001 | AS21 | 240 | Winter | 30 | +30% | 30/180 | Winter | | | | 48.358 |
| 4.002 | | | Winter | 30 | +30% | 30/180 | Winter | | | | 48.359 |
| 4.003 | AS23 | | Winter | 30 | +30% | 30/120 | Winter | | | | 48.346 |
| 5.000 | AS24 | | Winter | 30 | +30% | | | | | | 49.546 |
| 6.000 | AS26 | | Winter | 30 | +30% | | | | | | 49.828 |
| 5.001 | AS25 | | Winter | | +30% | | | | | | 48.732 |
| | | | | 1 | ©1082-2 | 015 Y | D GOL | itions | | | |

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|----------------------------|---------------------|-----------|
| Kingston House | | , |
| Long Barrow Road | | ~ |
| Orbital Park Ashford | | Mirro |
| Date 24/04/2018 14:34 | Designed by andrewb | Drainage |
| File PHASE 1 SW REV.MDX | Checked by | Didiridge |
| Causeway | Network 2015.1 | |

Summary of Critical Results by Maximum Level (Rank 1) for Storm

| | US/MH | Surcharged Depth | Flooded Volume | Flow / | Overflow | Pipe Flow | | Level |
|----------------|--------------|---------------------|-------------------|--------|----------|--------------|--------------------------|----------|
| PN | Name | (m) | (m³) | Cap. | (1/s) | (1/s) | Status | Exceeded |
| 1.000 | ASV2 ASV1 | 0.258 | 0.000 | 0.13 | | 4.8 15.2 | SURCHARGED SURCHARGED | |
| 1.001 | AS1 | 0.561 | 0.000 | 0.59 | | 22.7 | SURCHARGED | |
| 2.000 | AS13 | -0.139 | 0.000 | 0.31 | | 14.2 | OK | |
| 2.001 | AS14 | -0.076 | 0.000 | 0.74 | | 37.4 | OK OK | |
| 2.002 | AS15 | -0.012 | 0.000 | 0.53 | | 23.3 | SURCHARGED | |
| 2.003 | AS16 | 0.094 0.828 | 0.000 | 0.30 | | 58.5 | SURCHARGED | |
| 1,003 | AS2 AS17 | -0.054 | 0.000 | 0.26 | | 10.2 | OK | |
| 3.000 | AS18 | 0.134 | 0.000 | 0.27 | | 20.0 | SURCHARGED | |
| 3.002 | AS19 | 0.697 | 0.000 | 0.37 | | 20.0 | SURCHARGED | |
| 1.004 | AS3 | 0.842 | 0.000 | 0.13 | | 78.9 | | |
| 1.005 | AS4 | 0.944 | 0.000 | 0.11 | | 31.9 | SURCHARGED | |
| 1.006 | AS5 | 0.962 | 0.000 | 0.02 | | 31.7 | | |
| 4.000 | | 0.008 | 0.000 | 0.00 | | 1.5 | SURCHARGED SURCHARGED | |
| 4.001 | AS21 | 0.023 | 0.000 | 0.01 | | 3.7 | SURCHARGED | |
| 4.002 | | 0.049 0.076 | | | | 4.1 | | |
| 4.003 5.000 | | | | | | 13.6 | OK | |
| 6.000 | | | | | | 7.8 | OK | |
| 5.001 | | -0.833 | | | | 42.4 | OK | |

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|----------------------------|---------------------|-------------|
| Kingston House | | |
| Long Barrow Road | | 4 |
| Orbital Park Ashford | | Milesso |
| Date 24/04/2018 14:34 | Designed by andrewb | Designation |
| File PHASE 1 SW REV.MDX | Checked by | Drainage |
| Causeway | Network 2015.1 | |

Summary of Critical Results by Maximum Level (Rank 1) for Storm

| PN | US/MH Name | S | torm | | Climate Change | First Surc | t (X) harge | First (Y) Flood | First (Z) Overflow | Overflow Act. | Water Level (m) |
|-------|---------------|-----|--------|----|-------------------|---------------|----------------|--------------------|-----------------------|------------------|-----------------------|
| 1.007 | AS6 | 180 | Winter | 30 | +30% | 30/30 | Winter | | | | 48.341 |
| 7.000 | AS27 | 240 | Winter | 30 | +30% | | | | | | 48.163 |
| 1.008 | AS7 | 240 | Winter | 30 | +30% | 30/15 | Summer | | | | 48.163 |
| 1.009 | AS8 | 240 | Winter | 30 | +30% | 30/30 | Winter | | | | 47.988 |
| 1.010 | AS9 | 240 | Winter | 30 | +30% | 30/60 | Summer | | | | 47.808 |
| 8.000 | AS28 | 240 | Winter | 30 | +30% | 30/120 | Summer | | | | 47.623 |
| 9.000 | AS30 | 240 | Winter | 30 | +30% | 30/120 | Summer | | | | 47.623 |
| 8.001 | AS29 | 240 | Winter | 30 | +30% | 30/60 | Summer | | | | 47.623 |
| 1.011 | AS10 | 240 | Winter | 30 | +30% | 30/30 | Winter | | | | 47.623 |
| 1.012 | AS11 | 240 | Winter | 30 | +30% | 30/15 | Summer | | | | 47.622 |
| 1.013 | AS12 | 240 | Winter | 30 | +30% | 30/15 | Summer | | | | 47.621 |

| | | Surcharged | Flooded | | | Pipe | | |
|-------|-------|------------|---------|--------|----------|-------|------------|----------|
| | US/MH | Depth | Volume | Flow / | Overflow | Flow | | Level |
| PN | Name | (m) | (m³) | Cap. | (1/s) | (1/s) | Status | Exceeded |
| | | | | | | | | |
| 1.007 | AS6 | 0.266 | 0.000 | 0.01 | | 26.1 | SURCHARGED | |
| 7.000 | AS27 | -0.022 | 0.000 | 0.01 | | 1.3 | OK | |
| 1.008 | AS7 | 1.303 | 0.000 | 0.01 | | 16.1 | SURCHARGED | |
| 1.009 | AS8 | 1.463 | 0.000 | 0.01 | | 15.1 | SURCHARGED | |
| 1.010 | AS9 | 1.523 | 0.000 | 0.01 | | 15.4 | SURCHARGED | |
| 8.000 | AS28 | 1.068 | 0.000 | 0.01 | | 6.1 | FLOOD RISK | |
| 9.000 | AS30 | 0.608 | 0.000 | 0.01 | | 1.8 | FLOOD RISK | |
| 8.001 | AS29 | 1.503 | 0.000 | 0.02 | | 11.2 | FLOOD RISK | |
| 1.011 | AS10 | 1.883 | 0.000 | 0.02 | | 19.0 | SURCHARGED | |
| 1.012 | AS11 | 2.087 | 0.000 | 0.02 | | 14.2 | FLOOD RISK | |
| 1.013 | AS12 | 2.836 | 0.000 | 0.39 | | 14.6 | FLOOD RISK | |
| | | | | | | | | |